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DEVELOPMENT OF AIR FORCE FLIGHT SAFETY MODELS. VOLUME 8. 0-2 AI--ETC(U)

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DEVELOPMENT OF AIR FORCE FLIGHT SAFETY MODELS

Volume 8

**AIRCRAFT** 

January 1976

Prepared for

SERVICE ENGINEERING DIVISION SAN ANTONIO AIR LOGISTICS CENTER Kelly Air Force Base, Texas

Under Contract F09603-72-A-1132-SA01

Publication C54-01-1-1406

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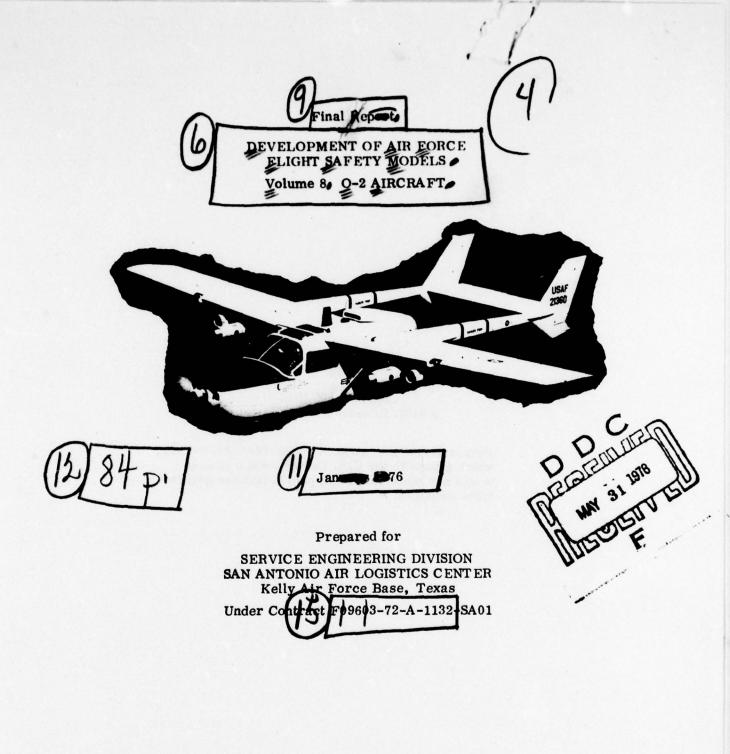
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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
I. REPORT NUMBER .	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
C54-01-1-1406 -			
DEVELOPMENT OF AIR FORCE FLIGHT SAFETY MODELS Volume 8		5. TYPE OF REPORT & PERIOD COVERED	
		6. PERFORMING ORG, REPORT NUMBER C54-01-1-1406	
7. Author(*) Not Listed		F09603-72-A-1132-SA01	
9. PERFORMING ORGANIZATION NAME AND ADDRESS ARINC Research Corporation  2551 Riva Road Annapolis, Maryland 21401		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
11. CONTROLLING OFFICE NAME AND ADDRESS SERVICE ENGINEERING DIVISION		12. REPORT DATE	
SAN ANTONIO AIR LOGISTICS CENTER		January 1976	
Kelly Air Force Base, Texas		45	
14. MONITORING AGENCY NAME & ADDRESS(II different SERVICE ENGINEERING DIVISION	t from Controlling Office)	15. SECURITY CLASS. (of this report)	
SAN ANTONIO AIR LOGISTICS CENTER Kelly Air Force Base, Texas		UNCLASSIFIED	
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UNCLASSIFIED/UNLIMITED  17. DISTRIBUTION STATEMENT (of the abstract entered	e in Block 20, if different fro	m Report)	
13. SUPPLEMENTARY NOTES			
19. KEY WORDS (Continue on reverse side if necessary an	d identify by block number)		
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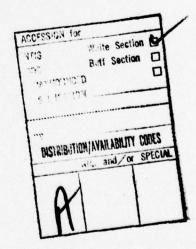
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### **ABSTRACT**

A general description of the Flight Safety
Prediction Technique, and the documentation
associated with its specific application to the O-2A
and O-2B aircraft, are presented.



#### **GLOSSARY**

This glossary presents general definitions of terms used in this report. The reader will find certain of these terms defined in somewhat different words in the text, depending on the context of the discussion; but the meaning will be consistent with the definitions given here.

Criticality	A numerical index of the significance of equipment failure history relative to aircraft safety. As an analysis param- eter, it can be considered proportional to the likelihood that an item will fail and thereby cause an accident. It is the product of the failure probability and the sensitivity of an equipment item.
	equipment item.

Dependency	-	See link	dependency.

FSPT	-	Flight Safety	Prediction	Technique
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Flight Phases	- Discrete segments of the aircraft mission profile. For
	present purposes, the flight phases are defined as 1) startup
	and taxi, 2) takeoff, 3) climb, 4) cruise, 5) tactics,
	6) cruise, 7) descend, 8) land, and 9) taxi and shutdown.

Functional Analysis	<ul> <li>The determination of equipment relationships to aircraft functions performed, and the interrelationships of these</li> </ul>
	functions.

Functional Link	- The simplest form of functional relationship in which one
	function is dependent upon the next lower function.

Functional Path	<ul> <li>The compilation of functional links, in sequence, through</li> </ul>
	which a function is identified as being dependent upon another.

Link Dependency	- The conditional probability of a dependent function failing,
	given that a particular function it is dependent upon has failed.

<b>Provisory Condition</b>	
	the safety-related importance of certain equipments is increased. Provisory conditions include icing, night flight,
	supersonic flight, etc.

Provisory Factor	- The probability that a provisory condition exists. Also used
	to describe the coded notation used to indicate that a functional
	relationship is dependent on a particular provisory condition.

Safety Sensitivity - Same as "sensitivity".

Sensitivity

- A quantitative indication of the degree of safety degradation to be expected if a function or piece of equipment fails. The more specific terms are "functional sensitivity" or "equipment item sensitivity".

Sensitivity Path

 A particular sequence of functional dependencies (beginning at the top level in the hierarchical structure) through which a function or piece of equipment derives a sensitivity value. Equipment and functional sensitivity values are often derived through several such sensitivity paths.

#### **FOREWORD**

This document is part of a 16-volume report describing the application to specific aircraft types of ARINC Research Corporation's Flight Safety Prediction Technique (FSPT). The technique was developed under previous Air Force contracts (see Appendix A). The present effort, undertaken in 1972 under Contract F09603-72-A-1132-SA01, has led to further refinement of the FSPT through its broad application to many different types of aircraft. The flight safety models generated for these aircraft are presented in individual volumes of this report as follows:

Volume	Aircraft	Volume	Aircraft
2	T-38	10	B-52G, H
3	F-111A, FB-111A	11	C-130E
4	A-7D	12	KC-135
5	F-4D, E; and RF-4C	13	C-5A
6	C-141	14	T-39
7	A-37	15	F-15
8	O-2	16	UH-1N Helicopter
9	OV-10		

Volume 16 will document the results of a feasibility study of extending the FSPT to rotary-wing aircraft.

Volume 1, an overall summary of the contractual effort, will be issued at the end of the contract period.

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The Flight Safety Prediction Technique developed by ARINC Research Corporation provides for assessment of the impact on flight safety of the failure of specific items of equipment within an aircraft. In the FSPT, mathematical modeling procedures are applied for processing aircraft-equipment failure data to yield a quantified index ranking safety-related problems on the basis of their likelihood of occurrence and the resulting degradation in the aircraft's capability to fly.

The ranking factor is called "criticality", which in its simplest form is the product of the failure probability and flight-safety sensitivity of an equipment. (A more detailed definition appears in Section 2 and Appendix B.) The failure probability inputs are from basic failure-data sources, AFM 66-1 and 65-110. The sensitivity estimates are derived by the following process:

- a. Systematic analysis of aircraft functions to determine those essential to flight safety
- b. Identification of the hardware required to perform these functions
- Evaluation of the safety significance of the hardware in performing these essential aircraft functions.

The criticality values resulting from this approach provide a relative ranking of all malfunctions with respect to their safety significance. Figure 1-1 is a simplified example of how three equipment items would be ranked on the combined basis of their failure probability and safety sensitivity. This figure illustrates an example in which item A has the highest failure probability, but due to the low sensitivity value is ranked below item B in criticality.

The methodology has the ability to rank malfunction problems currently and continuously by their accident potential. This ranking, based on criticality assessment, can provide the basic parameters necessary for:

- a. Identifying equipment items whose failure history and application pose a threat to aircraft safety
- b. Quantifying the degree of threat associated with each equipment item
- c. Evaluating and tracking the effectiveness of modifications to the aircraft
- d. Assessing safety benefits versus the cost of proposed aircraft modifications, changes in maintenance or flight operations, or alternative aircraft designs.

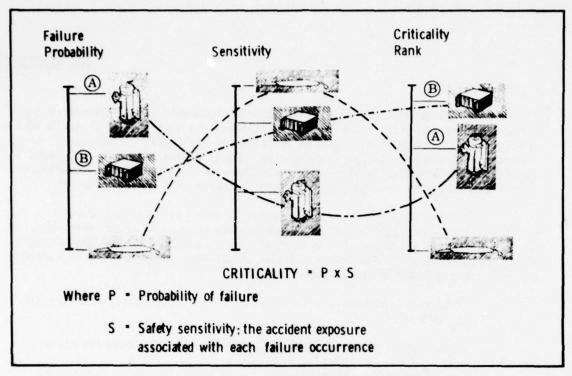


Figure 1-1. Example of Criticality Ranking Process

In this report, Section 4 and Appendix D pertain specifically to the O-2 aircraft. The remainder of the document provides support information that will make the O-2 data, and the method by which the data were obtained, more meaningful to the general reader.

Section 2 presents an overview of the development and utilization of the Flight Safety Prediction Technique; Section 3 discusses the steps associated with generating a safety model for calculating the safety criticality of various equipments of an aircraft; and Section 4 describes how the safety model for the O-2 aircraft was developed. Appendix A summarizes the contractual history of the development of the FSPT; Appendix B discusses mathematical considerations underlying the technique; Appendix C discusses FSPT documentation methods; and Appendix D presents functional relationship diagrams and a listing of keypunch cards that comprise the safety model documentation for the O-2 aircraft.

This section discusses the basic definitions and mathematical concepts associated with the Flight Safety Prediction Technique.

#### 2.1 DEFINITION OF SAFE AIRCRAFT

To develop a relative measure of aircraft safety degradation resulting from specific equipment malfunctions, it is first necessary to define a "safe" aircraft. For purposes of the FSPT assessments, an aircraft is assumed to be in a safe condition if it is operating within its prescribed performance limits. Conversely, an aircraft operating (or about to operate) outside these limits is considered to be unsafe — in a condition where property damage and personal injury may result.

The safety prediction methodology does not attempt to assess the extent of possible personal injury or aircraft damage resulting from an unsafe condition. Neither does the concept consider ejection capability, parachutes, life rafts, etc., which do not make an aircraft safer per se but provide for the survivability of the aircrew when the aircraft is unsafe. Collision is also excluded from consideration because of the complexity of the interrelationships between pilot, aircraft equipment, ground surveillance, and traffic density.

#### 2.2 MATHEMATICAL BASIS OF FSPT

The probability of an accident caused by the failure of an element can be expressed as the probability of the element failing multiplied by the conditional probability that the failure of the element will cause an accident. Stated in equation form:

$$P(A,j) = P(j)P(A|j)$$
 (1)

where

P(A,j) = Probability of an accident due to failure of just the jth element\*

P(j) = Probability that element j fails

P(A|j) = Probability of an accident given that the j<sup>th</sup> element fails.

This equation reflects the basic relationships addressed in the FSPT where:

- a. The criticality of the jth element is an estimate of P(A, j)
- b. The sensitivity of the jth element is an estimate of P(A|j)

<sup>\*</sup>In this and subsequent discussions, unless otherwise stated, expressions such as "failure of the jth element" should be interpreted to mean: failure of only the jth element, assuming all other elements are not failed.

Because an element's effect on safety may depend on the mission phase (see Section 3.2.1), the above model can be expanded to:

$$P(A,j) = \sum_{k=1}^{N} P_{j,k} P(A|j,k)$$
 (2)

where

N = Number of mission phases

P<sub>i,k</sub> = Probability that the j<sup>th</sup> element is failed in the k<sup>th</sup> phase

P(A|j,k) = The jth element's sensitivity in the kth phase.

To identify the importance of discrete elements to aircraft safety, a flight profile consisting of nine distinct phases was defined. The phases are discussed in Section 3.2.1.

To utilize equation 2, it was necessary to develop a method for obtaining the values of P(A | j, k), the probability that a malfunction in element j during mission phase k will result in an accident. This method in turn requires the estimation of two parameters: the probability of accident if a major function is not available during each mission phase, and the dependence of the major function on subfunctions and elements during each such phase\*. Each function and equipment item thus derives its sensitivity value from its relationship to the major function(s) dependent upon it.

#### 2.3 SENSITIVITY ASSIGNMENTS

A great deal of information is available on the causes of aircraft accidents, but little exists from which to make the sensitivity assignments [P(A|j)]. These assignments are therefore largely subjective, based on the analyst's knowledge of the system and any information he may have on previous accident history. The sensitivity assignments are reviewed (and revised as necessary) by an Air Force/contractor team working on a particular model to ensure that consistent criteria have been followed. The team review and negotiation of sensitivity assignments is the mechanism by which the value becomes sufficiently objective for use with the model. This negotiation considers all of those top level functions as a group and reassigns sensitivity values as necessary to assure that the most objective proportionality is attained for the particular aircraft model. The same major-function sensitivity values are used for major functions on all aircraft models where configuration and mission profiles permit.

The development of criticality rankings for the various elements (j's) is dependent upon the ability to quantify the failure probability [P(j)] and the element sensitivity [P(A|j)] for each element. Since the intent of the concept is to provide a relative safety ranking of all malfunctions, it is not necessary to develop absolute

<sup>\*</sup>For a more detailed discussion of the mathematics of the FSPT, see Appendix B.

values for P(A|j). If the sensitivity values developed are correct relative to each other, a proper criticality ranking will be established. It is intended that criticality be an index proportional to P(A,j) and therefore provide the same relative rank ordering of elements. The major reasons for proportionality, rather than equality, are:

- a. The FSPT does not account for the effect of extraordinary pilot intervention to prevent an accident in case of equipment malfunction.
- b. Criticality quantification was limited in its treatment of simultaneous occurrence of independent, primary failures.
- c. Operational and malfunction data yield only a proportional estimate of the required information.

While strict proportionality cannot be mathematically proven, it is believed that the criticality rankings provide reasonable relative measures of equipment problem potential.

Figure 3-1 summarizes the approach to the assessment of flight-safety criticality of aircraft equipment. The first contractor activity is the identification of all functions the aircraft is expected to perform and the determination of their interrelationships. Next, each functional relationship is documented; and then sensitivity assignments are made at the major functional levels (below these levels, link dependency values are estimated; see discussion, Section 3.2.2). This process is carried out until each work unit code associated with a major function has been identified with respect to the function performed and dependencies have been estimated. Computer processing calculates the safety sensitivity for each work unit coded item, combines these values with the operation and failure data input by the Air Force, and produces the equipment criticality ranking.

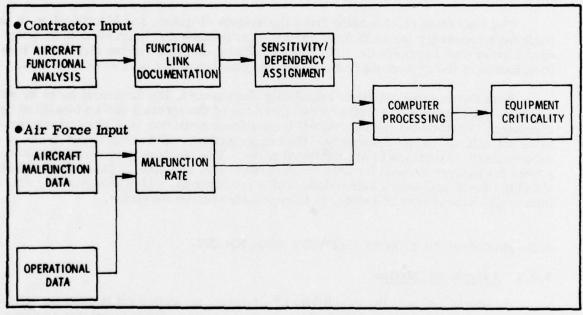


Figure 3-1. Activities and Data Inputs to Flight Safety Criticality Assessment

The steps in this process are discussed in greater detail in the following sections.

#### 3.1 FUNCTIONAL ANALYSIS

Functional analysis entails the systematic identification of the relationships of hardware to the functions performed by the aircraft and documented in the aircraft technical orders. Tabulated for each aircraft function are the equipments necessary for its performance as well as all outputs required for other systems. The complexity of the functional interdependencies of an aircraft requires the use of a systematic

accounting procedure, as discussed below, to assure that all relationships have been identified and that no functional paths have been overlooked.

Certain top-level functions (comprised of both "primary" and "major" functions) have been defined as applicable to all aircraft types, and serve as the starting point for a safety analysis. Figure 3-2 lists these top level functions with the primary function of Flight Control expanded to show its typical major functions. Below the major function level, differences in aircraft types result in function identification and structuring specifically suited to each aircraft. In Figure 3-2, for instance, the major function Roll Control is subdivided into Left Roll and Right Roll, and further into aileron and spoiler actuation subfunctions. This structure is that applicable to an F-4 aircraft, in which ailerons have an extremely limited upward travel and lift is primarily lost through spoiler operation. Finally, each item in the aircraft WUC ("-06") manual is identified with respect to the function it performs.\*

Every function and every WUC included in the model receives an "alpha designator" unique to that aircraft model. Due to the large number of alpha designators required in a model, an indenturing system is utilized to prevent duplication. However, the location in the hierarchical structure and the number of characters in the alpha designators are often independent, since such correlation is not necessary for subsequent computer processing.

The functional relationships from the system diagram, and identification of the equipment necessary for each function, are next documented in an 80-column punch-card format (see Appendix C). The total functional diagram for the aircraft is then a compilation of the system diagrams, with one punchcard for each functional link.

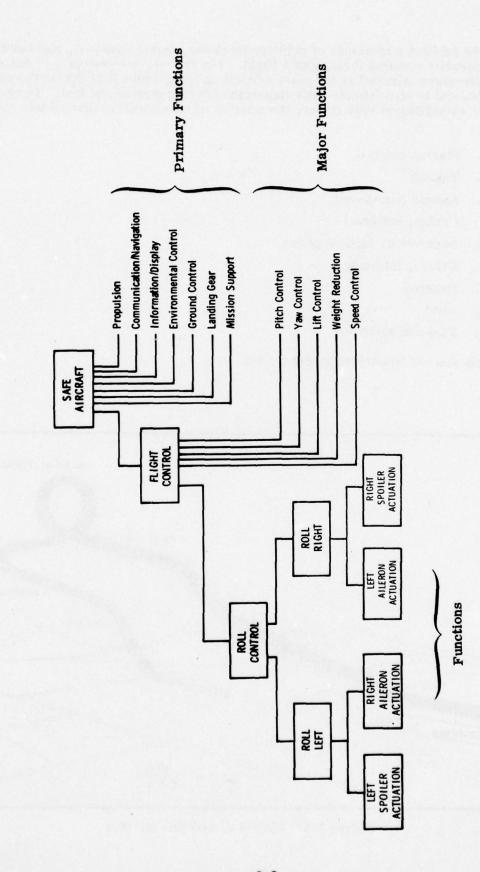
With the aircraft functions completely documented, the functional paths by which a piece of equipment contributes to the operation of the aircraft can be identified by computer. Performing the path-identification/documentation task by computer proves to be not only useful but necessary — the human analyst could neither keep track of nor assign sensitivity values to all functional paths. The machine processing capability allows the analyst to consider only one functional link at a time. The ability to follow all of the functional interrelationships within the aircraft, which is necessary for meaningful assessment of safety, is then provided by the computer.

#### 3.2 MAJOR-FUNCTION SENSITIVITY ASSIGNMENT

#### 3.2.1 Assignment Method

As stated earlier, the sensitivity of a function or equipment item is an estimate of the probability that its failure will cause an accident. From functional analysis of the aircraft under consideration, major functions are identified and are assigned sensitivity values for each phase of the mission.

<sup>\*</sup>Certain WUC items in the "-06" manual may not be included in the safety model, these items being either 1) eliminated by TCTOs; 2) purely structural items in the 11000 series; 3) necessary only for survivability or ejection; 4) of lower indenture than the LRU level, where computer data screening eliminates failure reports.



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Figure 3-2. Hierarchical Structure of Aircraft Functions

The relative importance of primary functions, major functions, and functions is not necessarily constant throughout a flight. The failure, for example, of one engine of a multi-engine aircraft is far more critical on takeoff than it is during the rest of the flight, and is of relatively little importance during startup and taxi. To accommodate this variability of importance, the mission of an aircraft is divided into nine flight phases:

- 1. Startup and taxi
- 2. Takeoff
- 3. Ascend (climb-out)
- 4. Cruise, outbound
- 5. Intercept or tactical phase
- 6. Cruise, inbound
- 7. Descend
- 8. Land
- 9. Taxi and shutdown

These phases are illustrated in Figure 3-3.

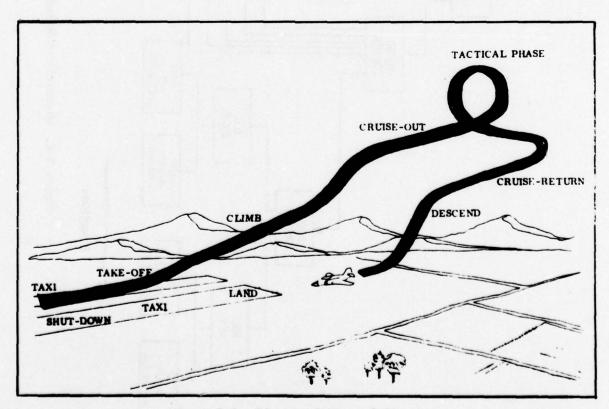


Figure 3-3. Phases of Aircraft Mission

A sensitivity value is assigned for each of the phases, and represents the best estimate of the likelihood that the aircraft will enter a hazardous mode if the function is not present in that phase. The numerical values assigned are proportional rather than absolute, and range from 0.0 to 1.0. The keypunch card format limits this assignment to increments of 0.1. Increments smaller than 0.1, when required, were assigned by defining a quasi-function for insertion between the major function and its dependent primary function.

#### 3.2.2 Link Dependency Assignment

"Link dependency" is defined as the probability that the loss of a function will result in the loss of a dependent function. (For a more detailed discussion of this term, see Appendix B.) The assignment of link dependency values requires knowledge of the operation of specific aircraft because it is concerned only with functional levels below the "major" category. At this lower level, no evaluation is made of the impact on flight safety of the loss of functions. Instead, the effect of the loss of one function on the performance of another function becomes the evaluation criterion. Like sensitivities, link dependency values are assigned in increments of 0.1. Additionally, the method of attenuation used in assigning sensitivity values can also be applied to link dependencies.

#### 3.2.3 Provisory Factors

The sensitivity of major functions with respect to aircraft safety, and at the lower levels the link dependency between functions, can be dependent on external influences and aircraft operating conditions. To accommodate these external influences, a set of provisory factors has been identified. An example would be a wind-shield anti-ice system, which has a safety sensitivity close to 1.0 during landing under icing conditions but a negligible effect on a dry, warm day.

Under such circumstances, the procedure is to assign the "worst case" value (assuming the condition exists). During model exercise the likelihood that the condition exists can be "read-in", thereby allowing the sensitivity value to be assigned by the computer based on the likelihood of the condition and the probability that the higher level function will therefore be lost. Table 3-1 lists the standard provisory factors used in FSPT models.

#### 3.2.4 Computer Processing

Documentation of a flight safety analysis by ARINC Research thus consists of functional diagrams, coded functional tabulations, a functional data processing card deck, and a machine-prepared printout of the card deck data. Under this contract, the documentation is then sent to San Antonio Air Logistics Center for review by MMER personnel and representatives of the Air Logistics Center responsible for the particular aircraft (if other than SA/ALC).

SA/ALC processes the functional data card deck utilizing a number of computerized operations. First, a functional deck edit is accomplished to identify certain format or logic errors that may exist. Next, a path identification/documentation run is made that traces all possible paths associated with each function and calculates the numerical sensitivities by flight phase down to the WUC level. Then, a path combination run is made taking into account the dependence of more than one major function on a particular WUC. Finally, failure information from the 66-1 data system and numerical factors for provisory conditions are input and a WUC criticality list by rank order is generated by the computer.

A B C D F	Icing conditions  Adverse speed/altitude operations  Runway stopping distance/confined area (Helicopter)  Night operation  IFR conditions
C D E	Runway stopping distance/confined area (Helicopter)  Night operation  IFR conditions
D E	Night operation IFR conditions
E	IFR conditions
F	
	Supersonic flight
G	Rain
н	Solo flight
ı	Loss of function for which indication is provided
к	Normal system failed
Т	Flame-out
x	Fire
Y	Cold weather
2	One of three available units is required
3	Two of three available units are required
4	One of four available units is required
5	Two of four available units are required
6	Three of four available units are required
8	Four of eight available units are required

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An additional product generated by the computer is a two-part criticality trend analysis. Part I contains the criticality rankings and linear regression analysis by WUC for the previous 12 months. Part II contains plots of the criticalities and regression lines for the 25 WUCs top-ranked according to safety criticality.

#### 3.2.5 Model Maintenance

Each time an aircraft type for which a safety model has been developed undergoes a modification, the effects of the changes on the model must be evaluated. Technical order and WUC revisions must be incorporated into the model. Removal of existing hardware, the installation of new hardware, or design improvements may change link dependencies and sensitivity assignments. The update procedure should follow the same general steps as outlined for the initial analysis effort.

Existing block diagrams and a printout of the functional card deck form the baseline for change identification. Functional relationships should be reviewed to determine the impact of changes on the documented safety analysis. Diagrams should be revised to reflect functional differences, WUC changes should be noted, and all differences listed on a flight-safety functional tabulation sheet. The functional deck printout can be used for manual indication of what the changes are and where they occur. New data cards are prepared and the functional deck updated by the removal of obsolete cards and the insertion of new cards. From this point on, the computer is again utilized to edit the functional deck, perform path identification/documentation, and calculate sensitivities for each WUC.

Block diagrams and other affected portions of the specific aircraft safety analysis report should be updated and revised pages issued that reflect these changes. Maintaining an accurate and updated model is important to obtaining an accurate assessment of the safety significance of hardware failures.

# 0-2 MODEL DEVELOPMENT

The FSPT model documented herein applies to the O-2A and O-2B aircraft. Model development on these aircraft was initiated in August 1974, and the completed documentation was submitted to SA/ALC for computer edit in January 1975.

The aircraft flight manual and maintenance technical orders provided the information on aircraft system operation. The model developed represents the O-2 aircraft configured to the latest time compliance technical orders (TCTOs) documented in the manuals supplied by SA/ALC. Table 4-1 lists the manuals and their revision status applicable to the developed model.

The O-2 safety model was developed by ARINC Research for all systems except the landing gear. The landing gear diagram and functional documentation cards were produced by MMER/SA/ALC, and interface documentation for the landing gear was a joint effort by SA/ALC and ARINC Research.

A single functional documentation deck having "O2" in columns 1 and 2 was used for the two versions of the O-2 aircraft. Cards having a blank in column 3 are common to both the O-2A and O-2B aircraft. When the common cards are combined with those having an "A" in column 3, the resulting deck documents the O-2A. Similarly, the common cards combined with the cards containing a "B" in column 3 document the O-2B.

Because of the vulnerability of the functional logic/sensitivity documentation to such errors as omission of links, duplication of cards, and keypunching, quality reviews were conducted at various critical points in the model development. In addition to keypunch verification, each card was checked against the functional link shown on the original rough draft and the final functional diagram and the diagrammed link was checked off. Missing or duplicated functional links were thus identified. Work unit codes used in the model were checked off against the WUC manual to assure completeness.

The quality reviews were first conducted by the organizations responsible for the subsystems prior to merging and computer verification of the respective aircraft decks by SA/ALC. Following the merging of the Air Force/ARINC Research decks and computer verification at SA/ALC, a second quality review was performed by representatives of ARINC Research and SA/ALC. Finally, the first criticality printout obtained from application of actual aircraft data was reviewed to identify any items whose sensitivity appeared to be unreasonable. In such cases the paths were traced manually and changes made if an erroneous relationship was found.

Appendix C presents the methods and standards used in documenting an FSPT aircraft model. Appendix D presents the FSPT documentation for the O-2 aircraft, which covers both the SA/ALC and ARINC Research portion of the model.

TABLE 4-1. O-2 SYSTEM DOCUMENTATION

Publication No.	Title	Revision/Date
1L-2A-1	Flight Manual	Basic, 1 Mar 1973
1L-2A-2	Maintenance	Change 9, 1 May 1971
1L-2A-6	Work Unit Code Manual	Change 3, 1 May 1974
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# APPENDIX A HISTORICAL SUMMARY OF FSPT

#### HISTORICAL SUMMARY OF FSPT

In 1965, the desirability and practicability of quantifying the significance of specific equipment malfunctions relative to flight safety was explored in a feasibility study conducted by ARINC Research Corporation for the Air Force. The feasibility of a safety-quantification approach, which has subsequently become known as Flight Safety Prediction Technique (FSPT), was demonstrated; and the method was developed and refined in a series of studies, as follows:

Study Phase	Subject/Date	Sponsor*/Publication No.
I	Feasibility Study, September 1965 to June 1967 (Phase I)	Sacramento Air Materiel Area (SMNE), Contract AF09(603)62335, SM-67-2; publication 705-01-1-777
II-A	Technique Development, October 1967 to July 1968 (Phase II-A)	San Antonio Air Materiel Area (SANEW), Contract AF09(603)-67-A-0267-SA01; publication 734-01-1-895
п-в	Technique Development, July 1968 to July 1969 (Phase II-B)	San Antonio Air Materiel Area (SANEW), Contract F09(603)-68-A-0317-SA01; publication 754-01-1-985 (Revision 1)
	FSPT System Documentation for the F-4C and T-37 Aircraft, October 1970 to June 1971	San Antonio Air Materiel Area (MMER) Contract F41608-71-C-0576; publication 697-01-1-1118

In the Phase II-B study, the FSPT was applied to the F-106 aircraft. Concurrent with Phase II-B, the U.S. Naval Safety Center contracted ARINC Research to extend the methodology to produce a flight safety criticality model for the F-4J aircraft. The results of this effort are documented in ARINC Research Publication 753-01-3-982 (Revision 1).

In 1970, ARINC Research was contracted to develop suitable input data to permit the application of the technique to the T-37 and F-4C aircraft. These data were derived in the form of mathematical model functional documentation as input to the basic computer program developed and applied to the F-106.

In 1972, ARINC Research Corporation was awarded a contract, with the subsequent modifications in 1973 and 1974, to apply the Flight Safety Prediction Technique to 15 aircraft, working jointly with cognizant Air Logistics Centers. Aircraft to which the FSPT has been applied under this latter contract (F09603-72-A-1132-SA01) include:

- a. T-38
- b. F-111A and FB-111A

<sup>\*</sup>The office symbols of Service Engineering at the Sacramento and San Antonio Air Materiel Areas are now SM/ALC/MME and SA/ALC/MME, respectively.

d. F-4D, E; RF-4C

e. C-141

f. A-37

g. O-2

h. OV-10

i. B-52G, H

j. C-130E

k. KC-135

l. C-5A

m. T-39

n. F-15

o. UH-1N Helicopter\*

<sup>\*</sup>Feasibility study of adaptation of FSPT to rotary-wing aircraft.

# APPENDIX B FORMULATION OF CRITICALITY-ASSESSMENT TECHNIQUE

#### FORMULATION OF CRITICALITY-ASSESSMENT TECHNIQUE

To implement the basic safety model defined in Section 2.2, it is necessary to develop a submodel for the probability that a malfunction in element j during mission phase k will result in an accident. This submodel in turn requires that we estimate two parameters: the probability of accident if a major function is not available during each mission phase, and the dependence of the major function on element j during each mission phase.

The first parameter is termed "functional sensitivity" and is estimated for each major function. The functional analysis performed in this task established for an aircraft the following hierarchal scheme:

Aircraft

Primary functions

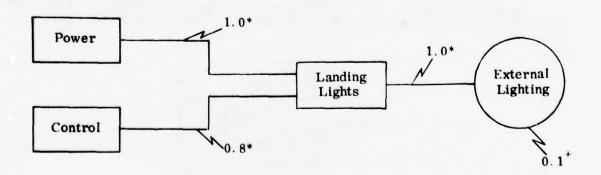
Major functions

**Function** 

Elements (Work Unit Codes)

A primary function would be one such as Flight Control. Major functions under Flight Control would include Pitch Control and Yaw Control.

The second parameter, "link dependency," is a vehicle for showing the influence of each functional-path element on the performance of a major function. For example, if the major function being considered is External Lighting, the following diagram illustrates the nature of functional sensitivity and link dependency values.



<sup>\*</sup> Link dependencies

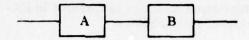
The 0.8 value means that failure of the Control function will result in loss of the Landing Light function 80% of the time. The 0.1 functional sensitivity value denotes that loss of external lighting will result in an accident 10% of the time. The values must be interpreted in a proportional sense, in that the actual accident probability is dependent upon external factors (see Section 3.2.3).

<sup>+</sup>Functional sensitivity

The remainder of this appendix discusses the procedures and model used to obtain element sensitivities; e.g., in the above example, the accident probability given that a Work Unit Code in the Control function malfunctions.

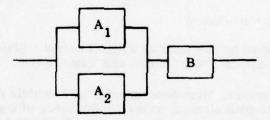
Three principal types of functional relationship—series, redundant, and parallel—were identified as representing the major forms to consider in modeling element sensitivity.

Series Relationship - A function having only one input. Schematically,



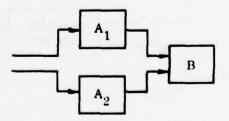
which indicates that outside of its own elements, the success of function B is only affected by the success of function A.

Functional Redundancy - A function having one or more backup functions that can provide the required inputs to successor functions. Schematically,



where A<sub>1</sub> and A<sub>2</sub> represent a functional redundancy in that either may provide the necessary input to B.

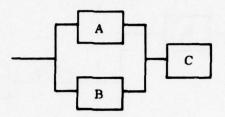
<u>Parallel Functions</u> — Two or more functions independent of each other in terms of functional success, but each of which may be required for a successor function. Schematically,



B will generally require both  $A_1$  and  $A_2$ ; but  $A_1$  does not depend on  $A_2$ , nor does  $A_2$  depend on  $A_1$ .

In some cases the distinction between functional redundancy and parallel paths is very slight, and may depend on mission phase. For example the four engines of a plane can be considered to be a redundant configuration providing inputs to the primary propulsion function during cruising, but would generally be considered to be parallel functions during takeoffs requiring full power.

In general, given a schematic relationship of the form,

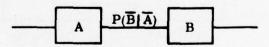


we can say that A and B are in a functionally redundant configuration if the success probability of C is the same if 1) A and B are successful, 2) A only is successful, or 3) B only is successful. If, for example, C is more likely to be successful if both A and B are successful, rather than A or B alone, then the relationship is one of parallel paths.

It is noted that the model will also account for element redundance and parallel elements through inputs such as  $P(\overline{A}|i_a)$ , representing the probability that the Ath function fails given that the  $i_a{}^{th}$  element in A has failed. If  $i_a{}^{th}$  is a parallel element, the probability would depend on mission requirements and other parallel-element states.

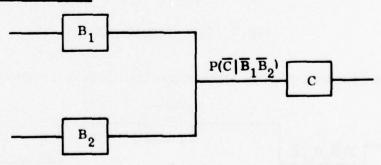
Link dependency is the conditional probability of a functional failure, given the failure of immediate predecessor functions. The link dependencies applicable to the three basic designs defined above are shown below.

#### Series Relationship

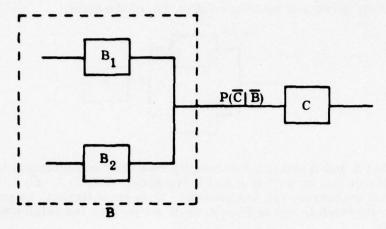


Link dependency =  $P(\overline{B}|\overline{A})$  = probability that B fails given that A fails.

#### **Functional Redundancy**

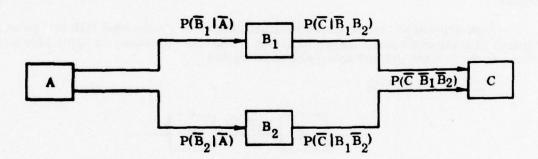


equivalent to



where  $\overline{B} = \overline{B}_1 \overline{B}_2$ 

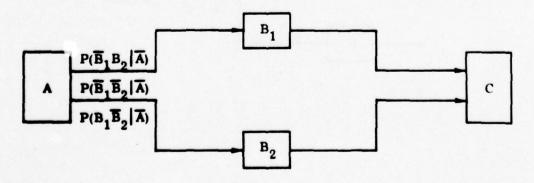
#### **Parallel Functions**



We shall generally assume that the dependencies of  $B_1$  with respect to A, and of  $B_2$  with respect to A, are independent of each other, so that

$$P(\overline{B}_1\overline{B}_2|\overline{A}) = P(\overline{B}_1|\overline{A})P(\overline{B}_2|\overline{A})$$

We then can consider three link dependencies from A to B as follows:



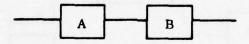
noting that

$$P(\overline{B}_1 | \overline{A}) = P(\overline{B}_1 B_2 | \overline{A}) + P(\overline{B}_1 \overline{B}_2 | \overline{A})$$

$$P(\overline{B}_2|\overline{A}) = P(B_1\overline{B}_2|\overline{A}) + P(\overline{B}_1\overline{B}_2|\overline{A})$$

Models are shown below for determining the sensitivity of elements within a function for each of the three basic designs. The following basic assumptions apply:

- a. Except for cases where an element has a redundant or parallel counterpart or is located in a function with a redundant or parallel function, only the element under consideration shall be assumed to have failed initially. Thus the expression  $P(A|i_a)$ , representing the accident probability given failure of the ith Work Unit Code element, is based on the assumption that no other element has failed unless element i is in some redundant or parallel configuration. For cases in which there are redundant or parallel counterparts, failures of such counterpart elements or functions are considered in accordance with their occurrence probabilities.
- b. The success of all immediate predecessors ensures the success of a function, provided that the function experiences no element failures. Thus for the series function relationship



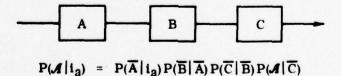
we assume

$$P(\overline{B}|A) = 0$$

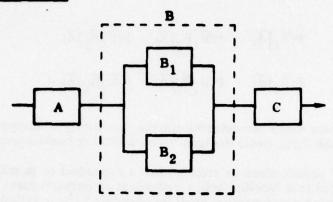
provided B experiences no element failures. If an element in function A is under consideration, the latter provision is always true by assumption

The element sensitivity models are:

#### Series Relationship



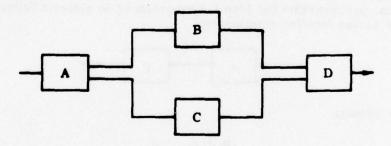
#### Functional Redundancy



 $P(\mathcal{A}|i_a) = P(\overline{A}|i_a)P(\overline{B}|\overline{A})P(\overline{C}|\overline{B})P(\mathcal{A}|\overline{C})$ 

 $P(\mathcal{A}|i_{b1}) = P(\overline{B}_1|i_{b1})P(\overline{B}_2)P(\overline{C}|\overline{B})P(\mathcal{A}|\overline{C})$ 

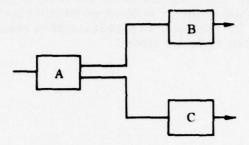
#### Parallel Functions



 $P(A|i_a) = P(\overline{A}|i_a) \{ P(\overline{B}C|\overline{A}) P(\overline{D}|\overline{B}C) + P(\overline{B}C|\overline{A}) P(\overline{D}|\overline{B}C) + P(\overline{B}C|\overline{A}) P(\overline{D}|\overline{B}C) \} P(A|\overline{D})$ 

 $P(A|i_b) = P(\overline{B}|i_b) \{ P(\overline{C}|i_b) P(\overline{D}|\overline{BC}) + P(C|i_b) P(\overline{D}|\overline{BC}) \} P(A|\overline{D})$ 

A case not explicitly incuded in the above three basic functional relationships is one for which a function is in two paths, e.g.,



then

$$P(\mathbf{A}|\mathbf{i}_{a}) = P(\overline{C}|\mathbf{i}_{a})P(B|\mathbf{i}_{a})P(\mathbf{A}|\overline{C}B) + P(C|\mathbf{i}_{a})P(\overline{B}|\mathbf{i}_{a})P(\mathbf{A}|C\overline{B})$$
$$+ P(\overline{C}|\mathbf{i}_{a})P(\overline{B}|\mathbf{i}_{a})\{1 - P(\overline{\mathbf{A}}|\overline{C})P(\overline{\mathbf{A}}|\overline{B})\}$$

where it is assumed that the effects of loss of the major functions in accident occurrence are independent of each other.

#### Use of Numerical Provisory Factors for Partially Redundant Systems

The numerical provisory factors (see Table 3-1) are used where more than two identical functions are involved in a redundancy. For example, aircraft with more than two engines often have identical and independent systems for hydraulic pressurization, and for electrical power generation, one driven by each engine. If the aircraft can be operated safely with one or more of such systems in a failed state, one of the numeric codes is utilized in assigning link dependency values. Consider, for example, the following:

If N identical and independent units\* are available and at least M are required for safe operation, where 0 < M < N, then the provisory factor of a given unit, say  $U_j$ , is the probability that the failure of  $U_j$  will cause the aircraft to enter an unsafe state. This is the probability that exactly M-1 of the remaining N-1 units will be in an unfailed state. This probability can be calculated by the formula for the binomial distribution, and is given by

$$P(U_j) = {N-1 \choose M-1} p^{(M-1)} q^{(N-M)}$$

where  $P(U_j)$  = probability that failure of the  $j^{\mbox{th}}$  unit will cause the aircraft to enter an unsafe state, and

M = Number of units required

N = Number of units available

p = Probability that a single unit will be in an unfailed state

q = Probability that a single unit will be in a failed state or (1-p)

<sup>\*</sup>Units may be either elements, element assemblies, or functions.

Assignment of link dependencies to N identical and independent units of which only M are required proceeds as follows. The value assigned to each unit is the dependency of the higher level function on receiving an output from M of the units (usually 1.0). The provisory factor is the appropriate numeric code. In the evaluation of the path sensitivity, the computer is programmed to select the binomial formula that corresponds to the provisory factor listed.

### APPENDIX C FSPT DOCUMENTATION METHODS

#### FSPT DOCUMENTATION METHODS

Because of the extreme complexity of aircraft, it is necessary to develop a computerized method to identify and document all possible paths associated with each function as well as to determine the safety sensitivity associated with each path. A computer routine has been devised that takes the data from the functional card deck and traces and documents all paths. For each WUC, it also computes the flight-phase sensitivities for each path in which the WUC is present. The resulting computer printout provides a combined functional path sensitivity.

#### C.1 ALPHA CODING

As each system of the aircraft is functionally diagrammed, the functional blocks are assigned an "alpha code". This code aids the analyst in the bookkeeping tasks of functional diagramming and provides the computer with an identification of the elements to be processed. For standardization among aircraft, nine top-level functions have been defined and each has been assigned an initial or first-alpha designator. Each block in the functional diagram carries the same initial alpha as the top level function. Subsequent letters added to the initial alpha uniquely identify each block.

The only restrictions placed on the assignment of alpha codes are that:

- a. All characters in a code must be a letter of the alphabet, and
- b. The maximum number of characters in one code is seven.

#### C.2 ALPHA CODING AND COMPUTER PROGRAM COMPATIBILITY

Additional rules for alpha coding required to obtain the desired results from computer processing include:

- a. When a WUC item operates in the same mode to perform more than one function, the same alpha code is used in each application.
- b. When a WUC item operates in a different mode to perform each of more than one function, a different alpha designator is assigned for each operating mode.

#### C.3 FUNCTIONAL TABULATION

The "Flight Safety Functional Tabulation" sheet is used to code the safety model for keypunching. The sheets are coded as follows (refer to Figure C-1) for an example).

a. Columns 1 through 3. Used to identify the aircraft represented by the model. For certain aircraft modeled under this contract more than one model – designation series MDS – was included. For instance, a single functional deck was created for four MDSs of the F-4 aircraft. Cards with "F46"\* in columns 1-3 were common to all aircraft. For example,

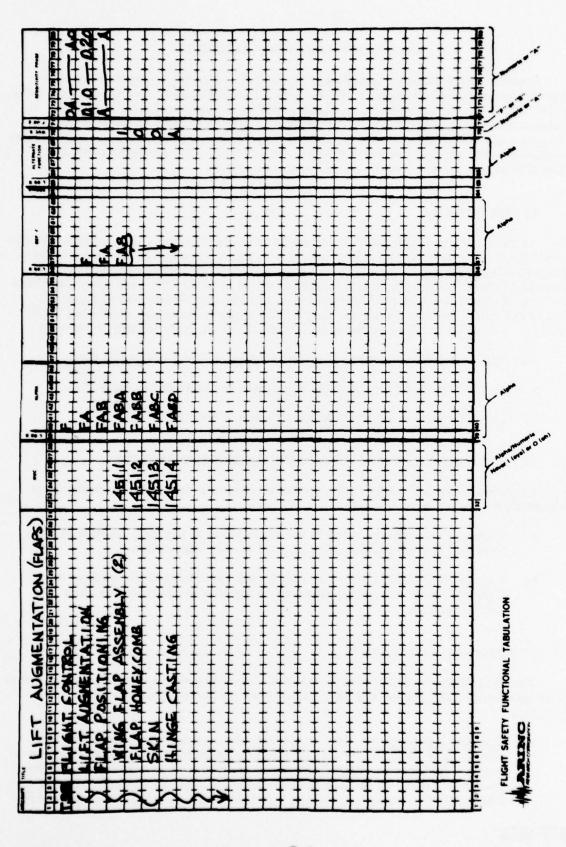


Figure C-1. Flight Safety Functional Tabulation

when these cards are combined with those carrying "F4E" in columns 1-3, then it produces an F-4E FSPT model deck.

- b. Columns 4 through 31. Contain the title of the function or the WUC item.
- c. Columns 32 through 36. Contain the left-justified WUC number.
- d. Columns 37 and 38. Blank
- e. Columns 39 through 46. Contain the assigned alpha designator for the function and/or the WUC. Column 39 contains either an L or an R, or is blank. The L and R designate left and right for those instances when the function and/or WUC pertains to the left or right side of the aircraft.
- f. Columns 47 and 48. Blank.
- g. Columns 49 through 55. Normally left blank, but are used after a deck is operational to substitute the data on a card for that stored in the computer by punching the line record number in this field.
- h. Columns 56 through 63. Identify the dependent functions for either the function or specific WUCs being coded. Column 56 may contain L, R or blank for the same purpose as that of column 39.
- i. Column 64. Contains the alphanumeric code of the "provisory factor" applicable to the link value assigned.
- j. Columns 65 through 69. Contain the alpha designator of a function that is an alternate for the function being coded. (Column 65 is used for "L" or "R" as in Column 39.) The presence of the "alternate alpha" flags the importance of the link dependency as being affected by the success probability of the alternate function.
- k. Column 70. Contains the work unit code dependency value (1 = 0.10; 2 = 0.20; ... A = 1.0). This value is applicable to all flight phases.
- l. Column 71. Contains special instructions to the computer through the use of letters F, S, or being blank. Cards with an "S" or "blank" in column 71 are used in sensitivity computations. Cards with an "F" document a functional relationships which, although present in the system, would produce an erroneous sensitivity value when combined with other nonindependent paths (having the same function in common at some higher level). The "F" prevents the computer from including the link in the sensitivity calculations.
- m. Columns 72 through 80. Contain functional dependencies for each of nine flight phases as described in Section 3.2.1 of the text. Coding is the same as for column 70.

#### C. 4 DIAGRAM CONSTRUCTION

The diagrams produced under the contract document the functional interrelationship of the aircraft systems considered in the model. In the interest of extending the useful life of the diagrams, WUC items are not shown, thereby eliminating the necessity of updating the diagrams with each (and sometimes frequent) change to the WUC manual.

As discussed earlier in this report, the diagrams represent the hierarchal structure of the paths from which the sensitivity values are derived. The diagrams, although consistent with the system schematic and reliability block diagrams, are not equivalent due to this hierarchal method of documentation. In the actual system, signals and/or fluids pass from one component to the next and are thus documented in schematics; conversely, the hierarchal approach only identifies the components that must operate to achieve a given function, independent of the direction and/or sequence of signal flow. This approach directly addresses the system impact of a component failure without the necessity of identifying the intrasystem secondary failures. Each line connecting functions on the diagram is documented by a punchcard, with the lower function providing the "alpha designator" and the higher function's alpha designator indicator as the "dependent function".\*

<sup>\*</sup>The card deck also documents functional relationships not shown on the diagram; the work unit codes (mentioned earlier) and the "S" cards discussed in paragraph C. 3. 1.

### APPENDIX D FSPT DOCUMENTATION OF O-2 AIRCRAFT

#### FSPT DOCUMENTATION OF O-2 AIRCRAFT

This appendix contains the functional relationship diagrams and a listing of the keypunch cards that comprise the FSPT safety model documentation for the O-2A and O-2B aircraft.

#### D. 1 DIAGRAMS

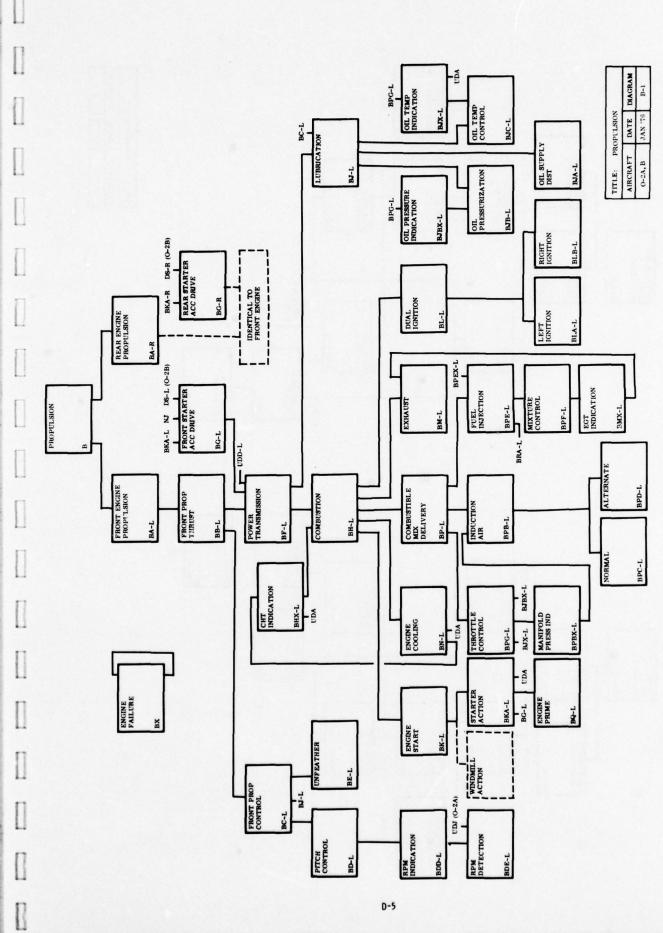
The diagrams illustrating the functional relationships considered in the O-2 safety model are presented on pages D-5 through D-16, and are listed below:

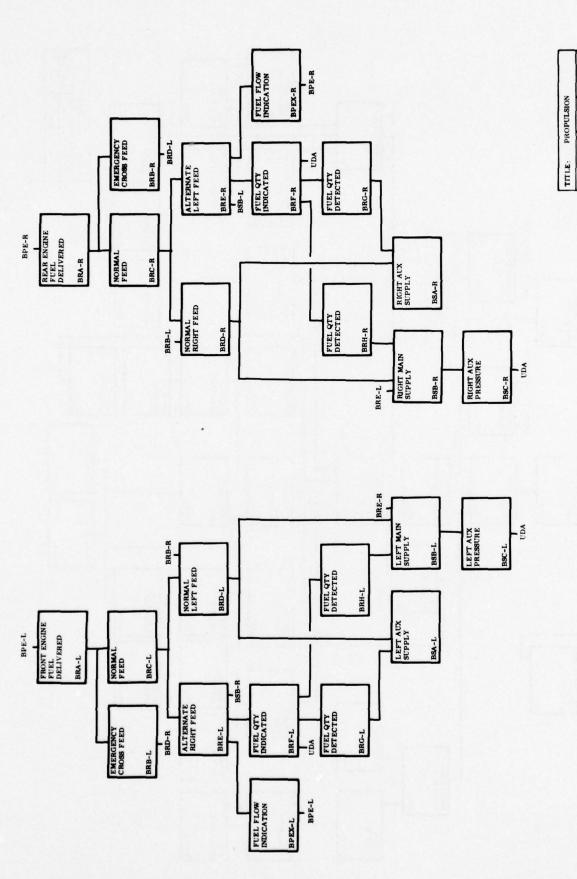
Title	Page
Propulsion, Diagram B-1	D-5
Propulsion, Diagram B-2	D-6
Comm/Nav/Ident, Diagram C-1	D-7
Comm/Nav/Ident, Diagram C-2	D-8
Information & Display, Diagram D-1	D-9
Environmental Control, Diagram E-1	D-10
Flight Control, Diagram F-1	D-11
Ground Control, Diagram G-1	D-12
Mission Support, Diagram M-1	D-13
Landing Gear, Diagram N-1	D-14
Utilities, Diagram U-1	D-15
Utilities, Diagram U-2	D-16

#### D. 2 CARD LISTING

Pages D-17 through D-44 are a reproduction of the punchcard listing. The listing is alphabetical by "alpha designator", and the format is that of the 80-column punchcard itself as described in Appendix C. At the top of each page the card columns are printed vertically; for example, column 34 is printed "4"

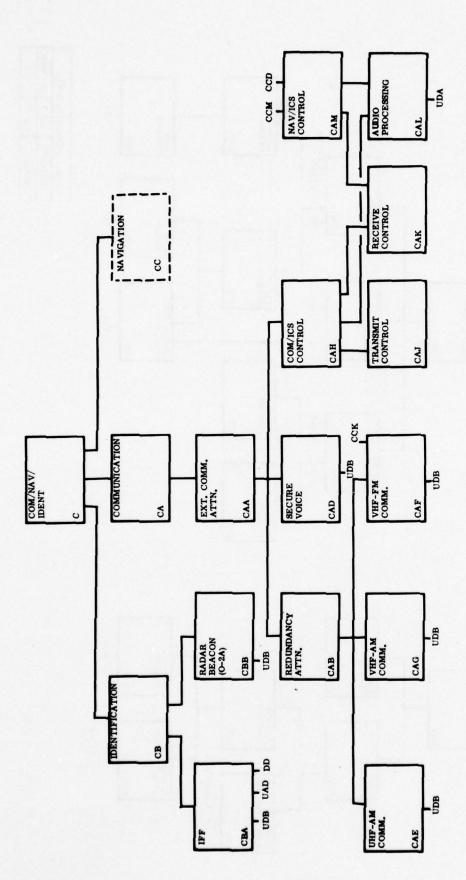
The first two columns of the punchcard are coded "O2". If the third column is blank, the card is common to both versions of the aircraft. Cards peculiar to one version of the aircraft carry a designator in column 3 for the aircraft - "A" for the O-2A and "B" for the O-2B.





 AIRCRAFT
 DATE
 DIAGRAM

 O-2A,5
 JAN 76
 B-2



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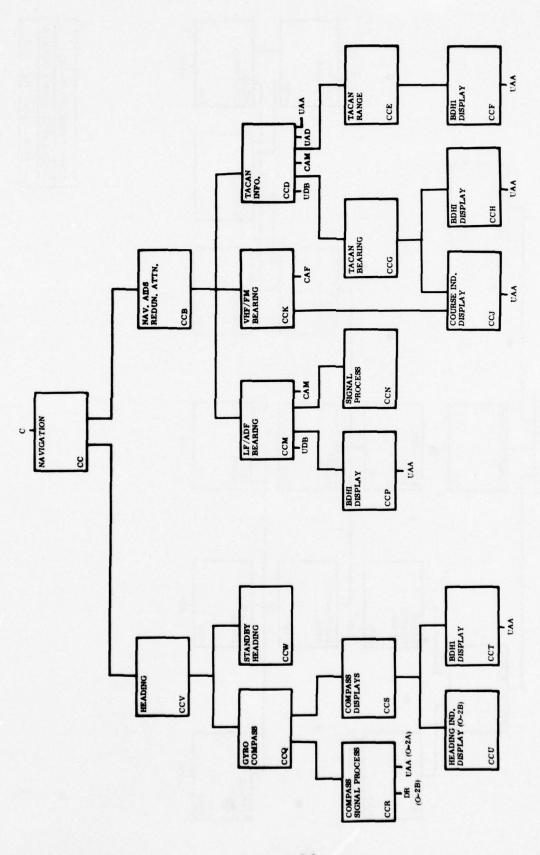
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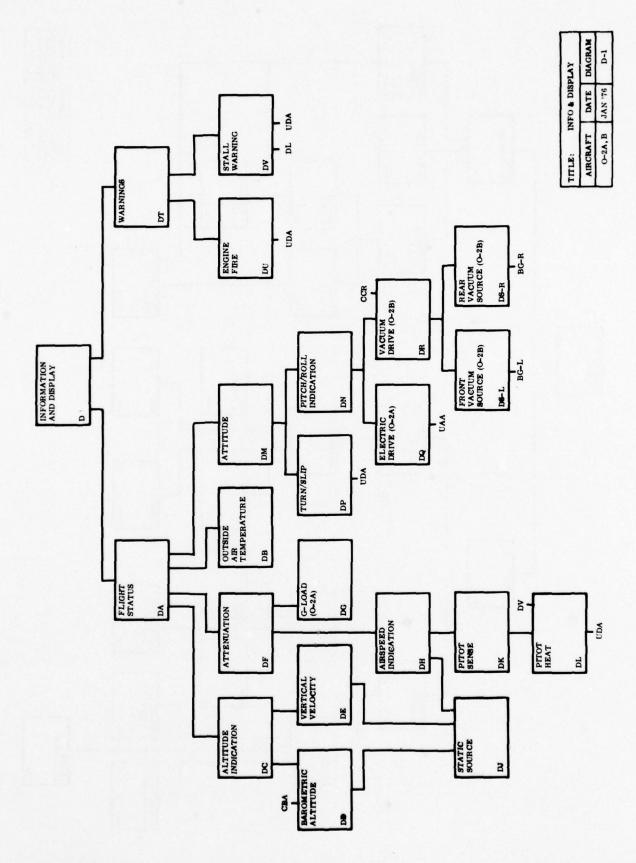


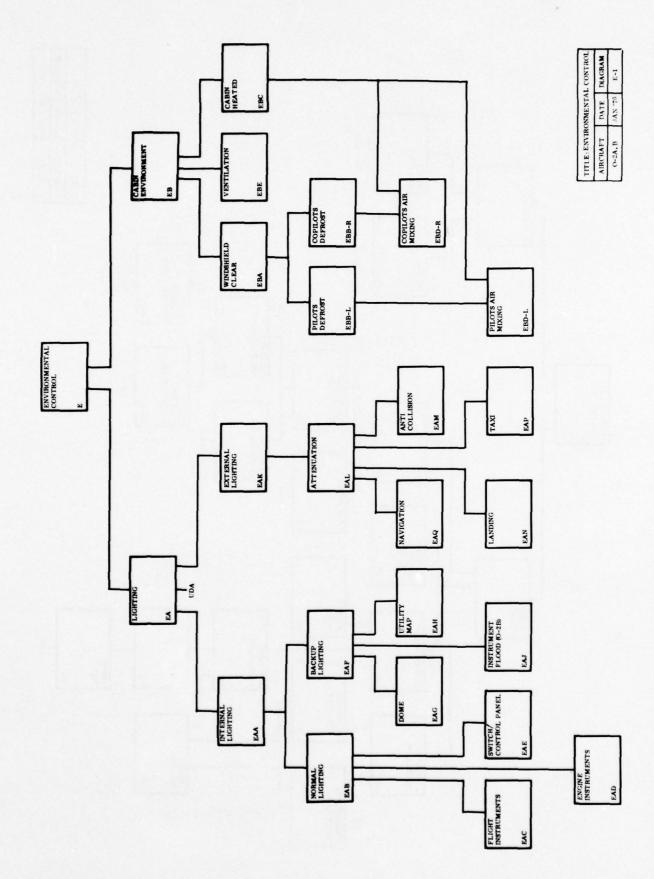


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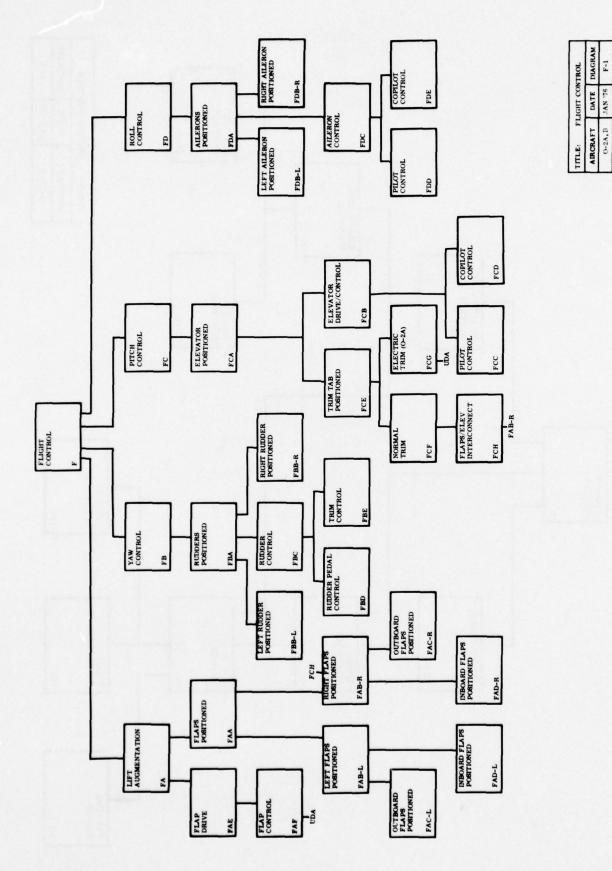
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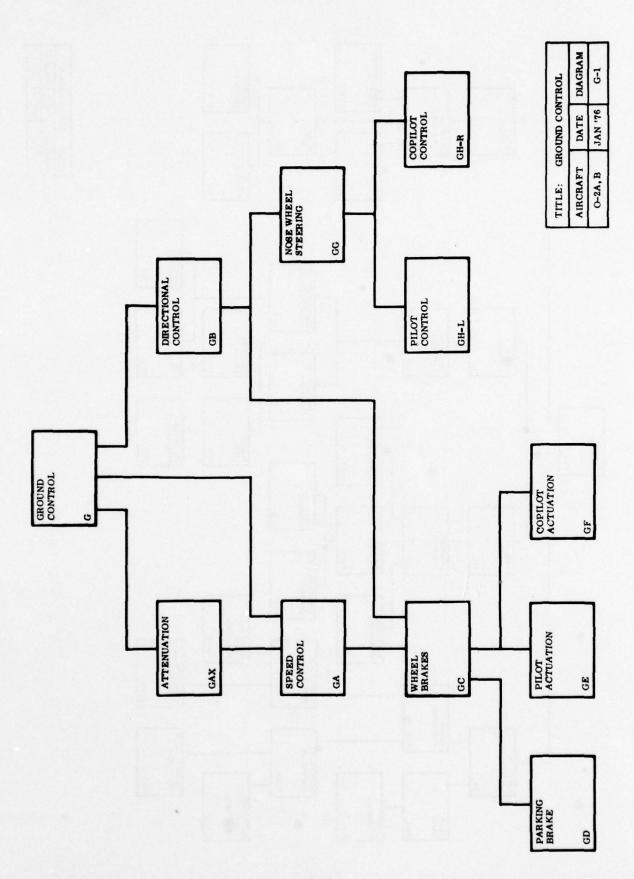


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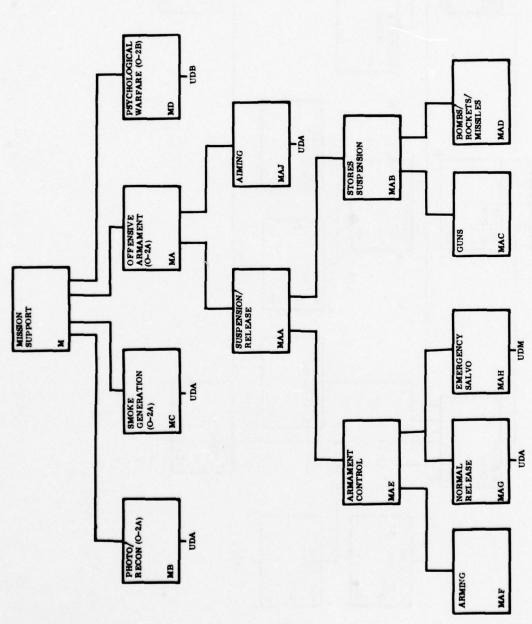


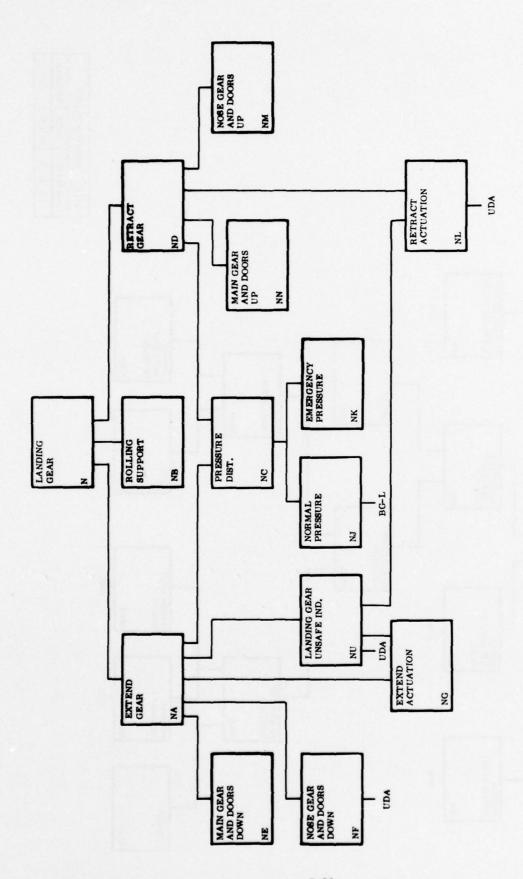
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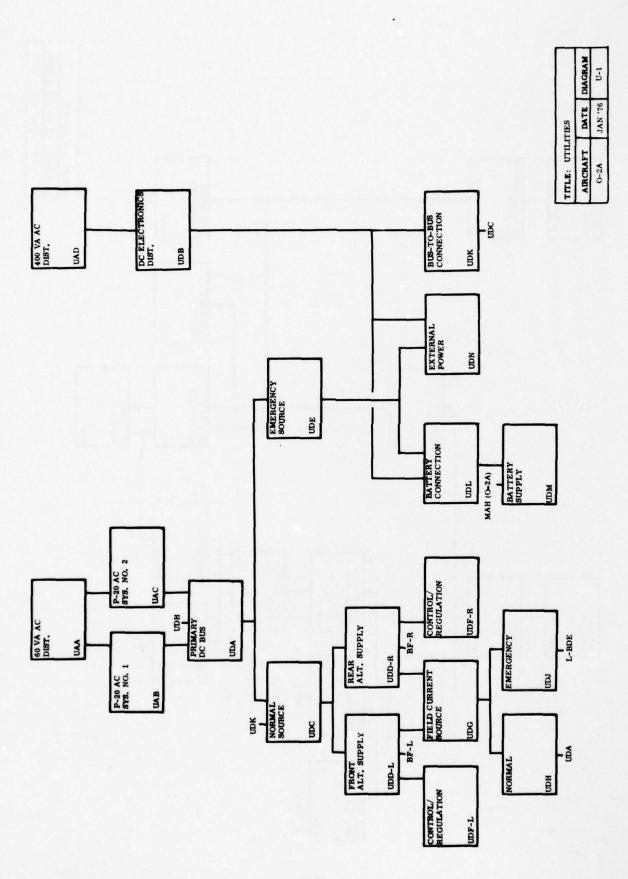
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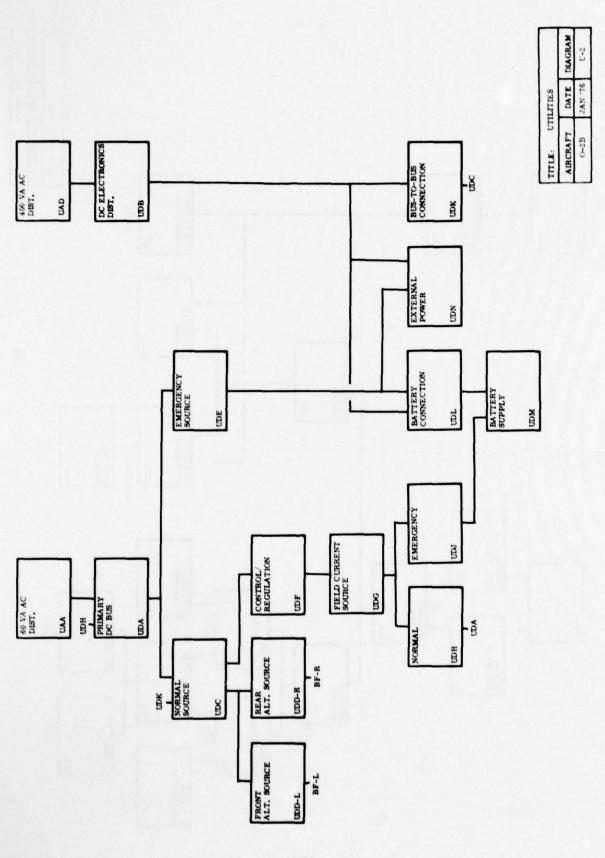


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	RONT ENGINE PROPULSION		LBA	H	K	HX		AAAAAAAA
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	FAR ENGINE PROPULSION		RBA	8				03000000
	SEAR ENGINE PROPULSION		484	R	K	HX		
12	ENGINE MOUNTS %4 FAC	21100	LHAA	LBA			Δ	
2	ENGINE MOUNTS #4 EAK	21100	RHAA	RBA			A	
12	SISCUITS &B EAC	21144	LBAB	LBA			0	
12	GISCUITS EB EAC	ALLIS	RAAH	RBA			0	
12	MOUNT ASSY- REAR	11AM1	RSAC	PRA			5	
	PROP THRUST	******	LEB	LBA				AAAAAAA
	PROP THRUST		K39	RBA				AAAAAAAA
,	PROP ASSY FRONT	SZAAO	LHBA	LBB			2	
2	PROP ASSY REAR	32 480	RBBA	898			2	
5	SLADE \$2 FAC	32444	LBBB	186			2	
2	BLADE	ABASE	RBBB	RAB			2	
2	BALANCE WEIGHT	32448	LBbC	LBB			5	
5	BALANCE WEIGHT	32A3B	RBBC	REB			5	
2	HUB ASSY	32 AAC	LBBD	LRS			2	
2	HU3 ASSY	32ABC	8880	RAR			2	
2	SPINNER ASSY	BEAAF	LBBE	Lan			O	
2	SPINNER ASSY	3246F	RBBE	868			5	
	POUP CONTROL	72.41)1	LBC	LBB			•	AAAAAAA
	PROP CONTROL		RBC	RHB				AAAAAAAA
2	CYL ASSY FEATHER	326A4	LBCA	LBC			Δ	
2	CYL ASSY FEATHER	32844	RBCA	RBC			A	
,	PIN.CYL LOCATING	326A6	LBCB	LBC			4	
2	PIN.CYL LOCATING	3284R	RBCB	980			A	
2	LATCH ASSY	SERAE	LBCC	LBC			5	
2	LATCH ASSY	32EAF	RBCC	3.90			5	
12	COUNTERWEIGHT	326AF	LBCD	LBC			A	
2	COUNTERWEIGHT	32BAF	RBCD	RBC			A	
2	LEVER ASSY	SZHAG	LBCE	1.80			2	
,	LEVER ASSY	328AG	RBCE	RBC			2	
2	TELEX PUSH-PULL	BZBAH	LBCF	LBC			2	
2	TILEX PUSH-PULL	HAHSE	RBCF	RBC			2	
2	GOVE RYOR	32FAJ	1865	L 3C			A	
2	GOVERNOR	326AJ	RBCG	RBC			A	
2	PUSH-ROD	328AK	LBCH	LBC			5	
2	PUSH-ROD	32EAK	RBCH	830			5	
2	SPEEDER SPRING	32 PAL	LBCJ	LBC			5	
12	SPEEDER SPRING	32FAL	KACJ	480			5	
2	GEAR PUMP DRIVE	328AM	LBCK	LBC			A	
2	GEAP . PUMP DRIVE	326AM	RHCK	RBC			A	
2	LIFT ROD	32FAP	LBCL	LPC			2	
2	LIFT ROD	BERAP	RUCL	PBC			2	
2	CONTROLEX	326AR	LBCM	LBC			5	
No.	CUNTROLEX	BERAR	RBCM	KBC			2	

PGG095.JIRL DATE = 01/12/76

	0300001111111111122 <i>2222222</i> 4567890123456789012345678					
112	PITCH CONTROL	.0123-201	LBD	LBC	. 34701070	AAAAAAAA
02	PITCH CONTROL		RAD	RHC		AAAAAAAA
112	STUP . FEATHERING	328AC	LBDA	LBD	0	
UZ.	STOP . FEATHER ING	328AC	RBDA	830	Ö	
(12	PLATE . LO PITCH STOP	32PAD	LBDB	LBU	ŏ	
12	PLATE, LO PITCH STOP	32PAD	RBDB	880	o	
02	VALVE RELIFF	32BAN	LBDC	1.80	8	
12	VALVE RELIEF	32EAN	RBDC	RBD	8	
112	RPM INDICATION	200	LBDD	L80	KLBPHX	111111111
12	RPM INDICATION		RADD	RBD	KRBPBX	111111111
12	TACH INDICATOR	21RA1	LBDDA	LBDD	8	
02	TACH INDICATOR	21RA1	RBDDA	R80')	8	
02	RPM DETECTION		LBDE	LROD		AAAAAAAA
UZA			LBDE	UDJ		AAAAAAAA
12	RPM DETECTION		RADE	RBDD		AAAAAAAA
72	TACH GENERATOR	ZIRAB	LBOEA	LBDE	A	
02	TACH GENERATOR	21RAB	RBDEA	RBDE	A	
02	FLEX SHAFT	21RAC	LBDEB	LBDF	A	
02	FLFX SHAFT	21FAC	RBDFB	RHUE	A	
C2	REDUCTION CRIVE	21FAD	LBDEC	LBDE	A	
112	REDUCTION DRIVE	21PAD	RBDEC	RROE	A	
52	DRIVE ADAPTER	21RAF	LBUED	LHDE	A	
112	DRIVE ADAPTER	ZIRAE	REDED	RBDE	A	
02	UNFEATHER		LBE	I. BC	T	AAAAAAAA
02	UNFEATHER		RBE	RBC	T	AAAAAAAA
72	ACCUMULATOR	32CAA	LBEA	LBF	A	
:12	ACCUMULATOR	32 CAA	RBEA	RBE	A	
02	UNFEATHER VALVE	32CAB	LBEB	LBE	۸	
02	UNFEATHER VALVE	32CAB	RBEB	RHE	Λ	
112	HOSE	32CAC	LBEC	LBE	A	
25	HOSE	32CAC	RREC	RRE	A	
02	POWER TRANSMISSION		LBF	LBB		ΑΛΑΛΑΔΑΔ
0.5	POWER TRANSMISSION		LBF	LBG		FAAAAAAAAA
92	POWER TRANSMISSION		LBF	LUDD		FAAAAAAAAA
U5	POWER TRANSMISSION		RBF	RBB		ΑΔΑΔΑΔΑΔ
U2	POWER TRANSMISSION		RBF	RBG		FAAAAAAAAA
02	POWER TRANSMISSION		RBF	RUDD		FAAAAAAAAA
12	CRANKCASE ASSY	21400	LBFA	LBF	1	
02	CRANKCASE ASSY	21400	RHFA	RBF	1	
0.5	HOUSING	21 444	LBFB	LRF	1	
0.2	HOUS ING	21444	RBFH	RRF	1	
OS	BREATHER	21448	I. BFC	LHF	٥	
02	HREATHER	21446	RBFC	RBF	0	
US	OIL SEAL	21848	LBFD	LBF	1	
US	OIL SEAL	21846	RBFD	RBF	1	
02	CRANKSHAFT ASSY	2184E	LBFE	LAF	۸	
12	CRANKSHAFT ASSY	218AE	RBFE	KBF	A	
02	CONNECTING ROD 76 FAC	21BAF	LBFF	LBF	8	
02	CONNECTING ROD %6 EAC	21845	RBFF	RHF	н	
0.5	CAMSHAFT AND GEAR	21BAK	LBFG	LAF	A	

GGU35.JIRI DATE = C1/12/76 00000000111111111112222222222	3333333	3344444444		REDICTION TECHNI:
2345678701234567890123456789	01234567	8901234567	890123456789012345	678901234567890
2 CAMSHAFT AND GEAR	21PAK	RBFG	RBF	A
2 FRONT ACCESSORY DRIVE		LRG	LBKA	ΑΑΑΑΑΑΑΑ
28 FRONT ACCESSORY DRIVE		LBG	LOS	ΑΛΑΛΑΛΑ
2 ACCESSORY DRIVE		LBG	NJ	ΑΔΑΔΑΔΑΛ
2 REAR ACCESSORY DRIVE		RBG	RBKA	ΑΑΑΑΑΑΑ
TH REAR ACCESSORY DRIVE		RBG	RDS	ΑΛΑΛΛΑΑΑ
2 ADAPTER-STARTER	21EAA	LAGA	LAG	Λ
ADAPTER-STARTER	21EAA	RBGA	RRG	Α
2 ADAPTER-START/ACC DRIVE	STEAB	LBGH	LBG	Α
2 ADAPTER-START/ACC DPIVE	21EAB	9868	RBG	A
2 CRANKCASE COVER ASSY	21EG0	LBGC	LBG	J
2 CRANKCASE COVER ASSY	51E 0C	RBGC	3 B G	0
2 COMBUSTION		LBH	LBF	
2 COMPUSTION		LBH	LBHX	FAAAAAAAA
2 COMBUSTION		RBH	RRE	ΑΑΑΑΑΑΑΑ
2 COMBUSTION		RBH	квих	FAAAAAAAA
2 CYLINDER ASSY %6 FAC	21000	LBHA	LBH	1
CYLINDER ASSY #6 EAC	21000	RBHA	RBH	1
2 VALVE, INTAKE %6 FAC	SICAC	LBHB	LBH	2
2 VALVE, INTAKE %6 EAC	SICAC	RBHB	RBH	2
EXHAUST VALVE %6 EAC	SICAD	LBHC	LBH	2
EXHAUST VALVE %6 EAC	SICAD	RBHC	квн	2
2 ARM-ROCKER % 12 EAK	21CAK	LBHD	LBH	1
ARM-ROCKER # 12 FAC	SICAK	RBHD	RBH	1
SHAFT-ROCKER #6EAC	SICAL	LnHE	LBH	ı
SHAFT-RUCKER #6FAC	SICAL	RAHE	квн	1
2 LIFTER-HYD %12 EAK	SICAN	LBHF	LBH	1
2 LIFTER-HYD \$12 EAK	SICAN	RBHF	RBH	1
2 ROD-PUSH 412 FAC	21CAP	LBHG	LBH	1
2 ROD-PUSH #12 FAC	21CAP	RRHG	RBH	1
2 PISTON ASSY %6 EAC	51000	LBHH	LBH	2
2 PISTON ASSY #6 FAC	21000	RBHH	я в н	2
2 PING	SIDAA	LBHJ	LBH	1
2 RIMG	SIDAA	RAHJ	RBH	1
2 PIN %6 EAK	SIDAB	LBHK	LBH	2
PIN #6 EAK	STOAR	RBHK	रहम	2
2 CHT INDICATION		LBHX	LBN	111111111
2 CHT INDICATION		RAHX	RBN	111111111
24 GAGE, COMBINATION	SIPCI	LBHXA	LRHX	A
24 GAGE, COMPINATION	21RC1	RSHXA	RBHX	Δ
ZA BULB, CHT	21RCC	<b>L</b> BHXB	LHHX	4
ZA HULB, CHT	SIRCC	RBHXB	RBHX	Δ
2H GAGE/PROBE ASSY	21FE1	LPHXC	LBHX	Α
28 GAGE/PROBE ASSY	21RE1	RBHXC	RBHX	Α
LUBRICATION		LBJ	LRC	FAAAAAAAAA
LUHRICATION		LBJ	LBF	019999910
2 LUBRICATION		RBJ	RRC	FAAAAAAAAA
LURRICATION		RHJ	RHF	019999910
2 OIL SUPPLY/DIST		LAJA	LBJ	ΔΑΔΑΛΑΔΑΔ
2 TIL SUPPLY/DIST		ABJA	RBJ	

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000	00000011111111112222222222 456789012345678901234567850	3333333	33444444444445555	555555666	6666666	577777777778
32	SUMP ASSY	21K00	LBJAA	LBJA	313010	3
112	SUMP ASSY	21K00	RHJAA	RBJA		3
112	PLUG	21KAA	LBJAB	LBJA		1
72	PLUG	21KAA	RBJAB	RRJA		i
1)2	SCREENS	21HAA	LBJAC	LBJA		Ō
32	SCREENS	21HAA	RBJAC	RBJA		C
02	PRESSURIZATION		LBJB	LBJ		AAAAAAAA
02	PRESSURIZATION		LBJB	LBJBX		FAAAAAAAA
02	PRESSURIZATION		RBJB	RBJ		AAAAAAAA
02	PRESSURIZATION		RBJB	RBJHX		FAAAAAAAAA
112	COVER OIL PUMP GEAR	21FAC	LBJBA	LBJB		Ó
22	COVER OIL PUMP GEAP	21EAC	RBJBA	RBJR		0
02	GEAR OIL PUMP DRIVE	21HAC	LBJBB	LHJR		8
02	GEAR . DIL PUMP DRIVE	21HAC	RBJBB	RBJB		8
02	PUMP	21HAD	LBJHC	LBJB		8
:12	PUMP	21HAD	RBJBC	RBJB		8
02	COVER OIL PUMP DRIVE	21HAE	LAJAD	LBJB		0
12	COVER OIL PUMP DRIVE	21HAE	RBJAD	RAJE		0
02	VALVE-PRESSURE RELIEF	21HAF	LBJBF	LBJB		3
02	VALVE-PRESSURE RELIEF	21HAF	RBJHE	RBJB		3
n2	OIL PRESS INDICATION		LBJBX	LRPG	ILBJ8	44444444
02	DIL PRESS INDICATION		RBJBX	RBPG	IRBJB	44444444
ASC	GAGE COMBINATION	21FC1	LBJBXA	LBJBX		A
024	GAGE COMBINATION	21FC1	RBJBXA	RBJBX		A
UZH	GAGE OIL PRESS	21RF1	LBJBXB	LBJBX		A
028	GAGE OIL PRESS	21RF1	RBJBXB	RBJBX		A
024	CKT BKR CUMBO GAGE	42FAB	LBJRXC	LBHX		A
OZA	CKT BKR COMBO GAGE	42FAB	LBJBXC	LBJX		A
1124	CKT BKR CUMBO GAGE	42FAB	RBJBXC	RAHX		A
721	CKT BKR COMBO GAGE	42FAB	RBJRXC	RAJX		A
02	DIL TEMP CONTROL		LRJC	LBJ		008888800
112	DIL TEMP CUNTROL		LBJC	LBJX		FAAAAAAAAA
172	DIL TEMP CONTROL		RBJC	RBJ		008888800
02	DIL TEMP CONTROL		RBJC	RBJX		FAAAAAAAA
02	CUOLER	21HAB	LBJCA	LBJC		5
02	COULER	SIHAB	RBJCA	RAJC		5
22	VALVE-VERNATHERM	21HAG	LBJCB	LBJC		5
(12	VALVE-VERNATHERM	21 HAG	RBJCB	RBJC		5
102	OIL TEMP INDICATION		LBJX	LBPG	IT 97C	33333333
172	OIL TEMP INDICATION		RAJX	RBPG	IRBJC	33333333
024	GAGE, COMBINATION	21 RC 1	LBJXA	LBJX		A
OZA	GAGE, COMBINATION	21RC1	AHJXA	KBJX		A
324	BULB DIL TEMP	21RCB	LBJXB	<b>LBJX</b>		A
157	BULB OIL TEMP	21FCB	RBJXB	RAJX		A
112H	GAGE / PROBE ASSY	21PD1	LBJXC	LBJX		A
n2H	GAGE / PROBE ASSY	21 RD1	RBJXC	RAJX		Α
112	ENGINE START		LBK	LBH	Ī	AAAAAAAA
.12	ENGINE START		RBK	явн	T	AAAAAAA
12	STARTER ACTION		LBKA	LHK		111111111
02	STARTER ACTION		RBKA	FRK		111111111

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J000J000011111111111222222222	3333333	33444444	4445555555556	666666666	777777778
123456789012345678901234567890	1234567	890123456	78901234567890	1234567890	1234567890
112 STARTER	21544	LBKAA	LRKA	Δ	
STARTER	21 SAA	RBKAA	RHKA	<b>A</b>	
02 CONTRACTOR	21 SAC	LBKAB	LBKA	Λ	
12 CONTRACTOO	21SAC	RBKAB	RBKA	Δ	
1124 ENGINE STARTER BUTTON	9921A	LBKAC	LBKA	4	
1124 FNGINE STARTER BUTTON	99214	RBKAC	PBKA	Δ	
028 MAGNETO/STARTER SWITCH	99218	LBKAD	LAKA	4	
028 MAGNETO/STARTER SWITCH	99218	RBKAD	RBKA		
026 CKT BKR INST CLUSTER	42FAB	LBKAE	LBHX	Δ	
OZB CKT BKR INST CLUSTER	42FAB	LBKAE	LAJX	Δ	
DZ CKT BKR START CONTROL	42 FAB	LBKAE	LBKA	Δ	
124 CKT BKR INST CLUSTER	42FAB	RBKAE	RBHX	Δ	
1125 CKT BKR INST CLUSTER	42FAB	RBKAE	RRJX	Δ	
02 CKT BKR START CONTROL	42FAB	RBKAE	RHKA	Δ	
02 CKT 3KR	42FAB	RBKAE	DU	Δ	
02 DUAL IGNITION		LBL	LBH		AAAAAAAA
02 DUAL IGNITION		RBL	RBH		AAAAAAAA
02 LEFT IGNITION		LSLA	I, BL	KL3L8	AAAAAAAA
02 LEFT IGNITION		RHLA	KHL	KRBLB	AAAAAAAAA
nz MAGNETO	21FAA	LBLAA	LBLA	A	
02 MAGNETO	21FAA	RBLAA	RBLA	A	
OZ SPARKPLUGS \$6 FAC	21FAC	LOLAB	LBLA	1	
OZ SPARKPLUGS %6 EAC	21 FAC	RBLAB	RBLA	1	
12 HARNESS	21FAB	LBLAC	LBLA	2	
02 HARNESS	21FAR	RBLAC	RBLA	2	
02 FILTER	21FAF	LBLAD	LBLA	2	
U2 FILTER	21FAF	RBLAD	RBLA	2	
02 MAGNETO SWITCH	9921R	LBLAF	LHLA	5	
02 MAGNETO SWITCH	9921B	RBLAE	FBLA	5	
12 RIGHT IGNITION		LBLH	L BL	KLBLA	AAAAAAAA
02 RIGHT IGNITION		RBLB	₹₿₺	KRBLA	4444444
nz MAGNETO	21FAA	LBLBA	LBLB	Δ	
02 MAGNETO	21FAA	RBLBA	RBLA	A	
12 SPARK PLUGS TE FAC	21FAC	LBLBB	L618	1	
UZ SPARK PLUGS \$6 EAC	21FAC	RBLBB	RBLB	1	
12 HARNESS	21FAR	TBT9C	LBLH	. 2	
112 HARNESS	21FAR	RBLBC	RHLB	2	
02 FILTER	21FAF	LBLBD	LBLB	2	
OZ FILTER	21FAF	SBLBD	BBLB	2	
02 MAGNETO SWITCH	99218	LBLBF	LBL3	5	
12 MAGNETO SWITCH	99218	RBLHE	RBLB	5	
02 EXHAUST		LAM	LBH		ΛΑΛΑΔΑΛΑΛ
12 EXHAUST		LBM	LBMX		FAAAAAAAAA
12 EXHAUST		RBM	RSH		
02 EXHAUST		RHM	RHMX		FAAAAAAAAA
UZ RISER FRONT %6 EAC	SINAV	LBMA	LBM	1	
12 RISER FRONT \$6 EAC	21NAA	FBMA	RBM	1	
G2 MUFFLER FRONT \$2 EAC	SINAD	LBMB	LBM	1	
02 MUFFLER FRONT \$2 FAC	21NAD	RHMH	RAM	1	
UZ SHRUUD ASSY FRONT #2 EAC	ZINAE	LBMC	LAM	0	

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				the state of the s	
02	SHROUD ASSY FRONT #2 EAC	21NAE	RBMC		
0.2	TAIL PIPE FRONT \$2 EAC	21NAF	LBMD		
0.2	TAIL PIPE FRONT \$2 FA	21NAF	RBMD	RBM	
(12	MOUNT SHOCK FRONT \$2 EAC	21NAH	LBME	L BM	
0.2	MOUNT SHOCK FRONT #2 EAC	21NAH	RBME	RBM	
0.5	COLLECTOR/BALL ASSY FRONT		LBMF	LBM	
02	COLLECTOR/BALL ASSY FRONT		RBMF		
02	RISER #6 EA< REAR	SINBA	LBMG	LBM	
0.5	RISER 86 FAC REAR	21NBA	RBMG	RBM	
(1)2	MUFFLER REAR	21NBD	LBMH	LBM	
112	MUFFLER REAR	SINBD	RBMH	RBM	
0.2	COLLECTOR/SOCKET ASSY REAR		LBMJ	LBM	
0.5	COLLECTOR/SOCKET ASSY REAR	Carried Control of the Control of th	RBMJ		
35	ELBOW/SOCKET ASSY REAR	21NHF	LBMK		
95	FLBOW/SOCKET ASSY REAR	21NBF	RBMK		
0.5	EGT INDICATION		LBMX	LBPF	000000000
112	EGT INDICATION		RBMX	RBPF	000000000
02	EGT INDICATOR	21FJ1	LBMXA		
112	EGT INDICATOR	21PJ1	RBMXA		
32	EGT PROBE	21FJA	LBMXB		
02	EGT PROBE	21RJA	RBMXB		
112	WIRING	21RJH	LBMXC		8
15	WIRING	21FJR	RBHXC	RBMX	3
32	ENGINE COULING		LAN	LBH	044111110
0.2	ENGINE COULING		RBN	RBH	044111110
0.2	CONL FLAPS #2 LAC	21PAA	LBNA	LBN	
<b>J2</b>	COWL FLAPS \$2 EAC	21PAA	RBNA	RBN	
02	SWITCH CONTROL	21PAC	LBNB		
0.2	SWITCH CONTPOL	21PAC	RAND	RBN	1
02	TORQUE TUBE	21 PAE	LBNC	LBN	1
112	TOROUE TUBE	21 PAE	RBNC	RBN	4
0.2	MOTOR	21PAF	LBND	LBN	1
112	MOTOR	21PAF	RBND	RBN	1
02	CONTROL RODS \$2 EAC	21PAG	LBNE	LBN S	5
72	CONTROL RODS #2 EAC	21 PAG	RBNE	R B N	5
22	SWITCH, LIMIT	21PAJ	LBNF	LRN	5
712	SWITCH.LIMIT	21PAJ	RBNF	RBN	5
25	AIRSCOOP ASSY TREARS	LIEBA	RBNG	RBN	
02	CYL BAFFLE ASSY	SICAT	LBNH	LRN	
32	CYL BAFFLE ASSY	21CAT	RBNH	KBN	
028	CKT 3KR COWL FLAPS	42FAB	LBNJ	LBN	1
325	CKT BKR COWL FLAPS	42FAR	RHNJ	PRN	4
112	COMBUSTIBLE MIX DELIVERY		LBP	LBH	AAAAAAAA
112	COMBUSTIBLE MIX DELIVERY		RBP	RBH	AAAAAAAA
12	AIR THROTTLE/FUEL METER AS	ZIGAB	LHPA	LBP	2
72	AIR THROTTLE/FUEL METER AS		RBPA		2
02	INDUCTION AIR		LBPB	LBP	AAAAAAAA
02	INDUCTION AIR		LBPB	LBPBX	FAAAAAAAA
02	INDUCTION AIR		RBPB	RRP	AAAAAAAA
22	INDUCTION AIR		KBPH	RBPHX	FAAAAAAAAA

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112	AIRBOX ASSY	21 JAC	LBPBA	LBPB	5	234301010
112	AIRBOX ASSY	21 JAC	RBPBA	RBPB	5	
UZ	MANIFOLD, FUTAKE	21JAJ	LBPBB	LRPB	í	
12	MANIFOLD, FUTAKE	21 JAJ	RBPBE	RBPS	•	
112	TURE ASSY	21 JAB	LBPBC	LBPB		
112	TUBE ASSY	21 JAB	RBPBC	RBPB	•	
12	AIR INDUCTION CONT LEVER	21MAE	LBPBD	LBPB	Δ	
02	AIR INDUCTION CONT LEVER			RBPB	A A	
02	AIR INDUCTION TELEFLEX	21MAE 21MAF	RBPBD	LAPA	A	
			LBPSF	RBPB	A	
02	AIR INDUCTION TELEFLEX	21MAF	RBPBE		KL BOD	11111111
02	MANIFOLD PRESS IND		LBPBX	LBPG		111111111
12	MANIFOLD PRESS IND	210. 1	RBPBX	RBPG	KR BU:)	111111111
02	GAGE, MAN PRESS	21RG1	LBPBXA	LBPBX	8	
02	GAGE MAN PRESS	21KG1	RBPBXA	REPBX	8	
1)2	NORMAL INDUCTION AIR		LBPC	LBPB	LBPD	111111111
02	NORMAL INDUCTION AIR		RBPC	RBPH	RBPD	111111111
02	FILTER	21JAA	LBPCA	LBPC	1	
02	FILTER	21 JAA	RBPCA	RRPC	1	
.12	ALTERNATE INDUCTION AIR		LBPD	LBPB	KL BPC	ΑΑΑΑΑΑΑΑ
0.2	ALTERNATE INDUCTION AIR		RBPD	RBPB	KRBPC	ΑΑΑΑΑΑΑΑ
02	DUCT ALT AIR	21 JAG	LBPDA	LBPD	0	
112	DUCT ALT AIR	21JAG	RRPDA	RBPD	0	
028	LEVER AIR INDUCTION CONTR		LBPOR	LBPD	A	
1126	LEVER AIR INDUCTION CONTR		RBPDB	RBPD	Δ	
023	TELEFLEX	21MAF	LBPDC	LBPD	4	
0.53	TELEFLEX	21MAF	RBPDC	RRAD	Α	
112	SPRING	21 JAK	LBPOD	LBPD	1	
0.2	SPRING	ZIJAK	RBPOD	RBPD	1	
0.2	FUEL INJECTION		LBPE	LBP		ΑΑΑΑΑΑΑΑ
(12	FUEL INJECTION		LBPE	LBPEX	f	- AAAAAAAA
32	FUEL INJECTION		RBPE	RBP		ΔΔΔΛΔΔΔΛ
112	FUEL INJECTION		RBPE	RAPEX	f	AAAAAAAA
0.2	PUMP/VAPOR SEP	21 GAA	LBPEA	LBPE	4	
2	PUMP/VAPOR SEP	21GAA	RBPEA	RBPE	4	
112	FUEL MANIFOLD VALVE	21GAC	LBPEB	LAPF	8	
22	FUEL MANIFULD VALVE	21GAC	REPER	RBPE	8	
CS	HOSE	21 GAD	LBPEC	LBPE	A	
02	HOSE	21GAD	RBPEC	RBPE	A	
112	NOZZLES %6 EAC	21GAE	LBPED	LBPE	2	
25	VOZZLES %6 EAK	ZIGAE	RBPED	RBPE	2	
12	TUBES	21 GAF	LAPEE	LBPE	8	
(12	TUBES	21 GAF	RHPEE	RBPE	8	
02	FUEL FLOW INDICATION		LBPEX	LBPE	ILBRD	111111111
0.2	FUEL FLOW INDICATION		RBPEX	RBRE	IRBRD	111111111
02	INDICATOR	21FH1	LBPEXA	LRPEX	A	
02	INDICATOR	21PH1	RBPEXA	RBPEX	A	
112	MIXTURE CONTROL		LBPF	LBPE		55555555
02	MIXTURE CONTROL		RBPF	RBPE		55555555
UZ	LEVER, MIXTURE	21MAC	LBPFA	LBPF	A	
112	LEVER, MIXTURE	ZIMAC	REPFA	RBPF	4	

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02	TELEFLEX 21MA		LBPFB	LBPF		Δ
02	TELEFLEX 21MA	N 21MAD	RBPFB	RRPF		1
112	CONTROLEX 21MA	D 21 MAK	LAPEC	LRPF		1
112	CONTROLEX 214A		RBPFC	RBPF		4
02	THROTTLE CONTROL		LBPG	LBP		ALAAAAAA
02	THROTTLE CONTROL		RBPG	646		AAAAAAAA
92	THROTTLE LEVER	21MAA	LBPGA	LAPG		4
72	THROTTLE LEVER	21MAA	RBPGA	RBPC		1
02	TELEFLEX 21	HAMIS LAM	LBPGB	LBPG		2
02	TFLFFLEX 21	MAJ 21MAB	RAPGA	RBPG		2
12	CONTROLEX 21	MAH 21MAJ	LBPGC	LBPG		2
112	CONTROLEX 21	MAB 21MAJ	RBPGC	REPG		?
35	ENGINE PRIMING		LBQ	LBKA	Y	511111111
0.2	HAGINE PRIMING		RHQ	RBKA	Y	511111111
02	PHIMING CONTROL	21UAA	LBQA	LBQ		
112	PRIMING CONTROL	21044	RBQA	PBQ		4
0.5	ENGINE FUEL DELIVERED		LBRA	LRPE		AAAAAAAA
1)2	ENGINE FUEL DELIVERED		KBRA	RBPE		AAAAAAAA
02	FUEL STRAINER	46LAH	LBRAA	LBRA		
112	FUEL STRAINER	46CAR	RBRAA	RBRA		
112	STRAINER DRAIN KNOB	46DAC	LBRAB	LBRA		
(15	STRAINER URAIN KNOB	46DAC	RBRAB	RBRA		)
:12	VAPOR RETURN CHECK VA		LBRAC	LBRA		
(,5	VAPOR RETURN CHECK VA	- Several Santa Market Santa S	RBRAC	RBRA		
02	HOSE- UNION/FIREWALL	46DAG	LBRAD	LBRA		3
02	HOSE- PUMP/UNION	46DAH	LBRAE	LBRA		8
32	HOSE- PUMP/FILTER	46DAJ	LBRAF	LERA		3
112	HOSE- FUEL FLOW	46DAK	LBRAG	LHRA		3
12	HOSE- PUMP/FIREWALL	46DAL	RBRAH	RBRA		3
0.5	HOSE- PUMP/FILTER	460AM	RARAJ	RHRA		3
02	HOSE - FUEL FLOW	46PAN	RBRAK	RBRA		3
02	EMERGENCY CROSS FEED		LBRB	LBRA	KLBRC	AAAAAAAA
02	EMERGENCY CROSS FEED		RBRB	RBRA	KRBRC	AAAAAAAA
25	VALVE	46EAF	LBRBA	LERS		
02	VALVE	46EAF	KARBA	RBRB		۸
02	NORMAL FEED		LBRC	LBRA	LBRB	111111111
02	NORMAL FEED SELECTOR VALVE	46CAD	RARC	KBRA LBRC	RBRB	111111111
012		400AD	RBRCA			
05	SELECTOR VALVE GEARBOX	46FAB	LBRCB	RARC LBRC		
02	GEARBOX	46EAB	RBRCB	RBRC		
02	HANDLE SELECTOR	46EAC	LBRCC	LARC		
112	HANDLE SELECTOR	46EAC	RBPCC	RRC		
02	CABLE FUEL SELECTOR	46EAD	LBRCD	LBRC		
112	CABLE FUEL SELECTOR	46 EAD	KBRCD	RBRC		
72	NORMAL LEFT FEED	TOLAU	LBRO	PARS		AAAAAAAA
02	NORMAL LEFT/RIGHT FEED		LBRD	LBRC	LBRE	111111111
32	NORMAL RIGHT FEED		RBRD	LBRB	Lune	AAAAAAAA
02	NORMAL LEFT/RIGHT FEED		RBRD	RBRC	RBRE	111111111
02	ALTERNATE LEFT/RIGHT F		LBRE	LBRC	KLBRD	AAAAAAAA
.,.	ACTEMIATI CE TITOTT			Cons		

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	00000011111111111222222222 45678901234567890123456789				
02	ALTERNATE LEFT/RIGHT FEED		RBRE	RBRC	KRBRD AAAAAAA
172	FUEL QTY INDICATED		LBRE	LBPF	111111111
02	FUEL OTY INDICATED		RHKF	KBRE	111111111
112	GAGE	46 GAA	LBREA	LBRF	8
1112	GAGE	40GAA	RARFA	RBRF	8
1128	SELECTOR SWITCH	46GAB	LBREB	LBRE	A
028	SELECTUR SWITCH	46GA8	RBREH	RBPF	A
112 A		46GAC	LBRFC	LBRF	Ā
024		46GAC	RARFC	HBRF	A
024	HANDLE SELECTOR	46EAC	LBRED	LARF	A
024	HANDLE SELECTOR	46 FAC	RARFO	RBRF	A
424	GEARBOX	46EAB	LBREE	LBRF	A
024	GEARBOX	46FAB	RBRFE	RBRF	A
	CKT 3KR COWLFLAPS	42FAB	LARFG	LRN	A
02	CKT BKR	42FAB	LBREG	LARF	A
	CKT BKR COWLFLAPS	42FAB	RBREG	RBN	A
02	CKT BKR	42FAB	RBREG	RBRF	A
02	FUEL DTY DET SAUX		LBRG	LBRF	22222222
02	FUEL DTY DET KAUX		RBRG	RHRF	222222222
02	TRANSMITTER. OTY AUX	46GAF	LBRGA	LBRG	8
02	TRANSMITTER . QTY AUX	46GAF	RBRGA	RBRG	ğ
112	FUEL QTY DETEMAINS		LBRH	LBRF	568868688
02	FUEL OTY DETEMAINS		RBRH	RBRE	8888888
112	TRANSMITTER SOUTBOX	46GAD	LBRHA	LBRH	8
112	TRANSMITTER &OUTEDS	46GAD	RBRHA	RBRH	8
12	TRANSMITTER SIN BOC	40GAF	LBRHB	LBRH	В
32	TRANSMITTER KIN BOC	46GAE	PBRHB	PBRH	8
02	AUX SUPPLY		LBSA	LPRD	222222222
72	AUX SUPPLY		LBSA	LPRG	FAAAAAAAA
112	AUX SUPPLY		RBSA	RBRD	222222222
72	AUX SUPPLY		RBSA	RBRG	FAAAAAAAA
02	AUX TANK ASSY	40CAA	LBSAA	LBSA	9
112	AUX TANK ASSY	46CAA	RRSAA	RASA	9
32	VALVE QUICK DRAIN	46CAC	LBSAB	LASA	1
02	VALVE QUICK DRAIN	46CAC	RBSAB	RBSA	1
02	MAIN SUPPLY		LBSB	LBRD	88888893
72	LEFT MAIN SUPPLY		LBSB	RBRÉ	ΑΑΛΑΛΑΛΑ
0.2	MAIN SUPPLY		LBSB	LBRH	FAAAAAAAA
0.2	MAIN SUPPLY		RBSB	RBRD	88888888
1,2	RIGHT MAIN SUPPLY		RHSB	LBRE	ΑΛΑΑΑΑΑΑ
02	MAIN SUPPLY		RBSB	RHRH	FAAAAAAAA
02	MAIN TANK ASSY	46AAA	LBSBA	LBSB	9
12	MAIN TANK ASSY	46444	RBSBA	RESB	9
02	HOSE INTERCONNECT	46AAC	LHSBB	LBSB	9
02	HOSE INTERCONNECT	46AAC	<b>КВВНН</b>	2854	9
02	VALVE VENT LINE CHECK	46AAD	LBSBC	LASB	3
112	VALVE VENT LINE CHECK	46AAD	RHSBC	RBSB	3
72	SUMP TANK ASSY	46HAA	LHSHO	LBSB	Δ
92	SUMP TANK ASSY	46RAA	<b>98580</b>	RBSH	Δ
112	VALVE QUICK DRAIN	46PAB	LBSBE	LBSB	1

CAE

CAE

CAF

CAG

CAE

CAE

CAB

CCK

CAF

CAF

CAF

CAF

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CAF

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FLIGHT SAFETY PREDICTION TECHNIQUE

UZ VALVE QUICK DRAIN	40PAB	RBSBE	PBSB	1
2 AUX PRESSURE		LRSC	LBSB	111111111
2 AUX PRESSURE		RBSC	RRSR	111111111
2 AUX PUMP	46LAA	LBSCA	LBSC	A
2 AUX PUMP	46DAA	RBSCA	RRSC	A
2 AUX PUMP SWITCH	40EAA	LBSCB	LBSC	A
2 AUX PUMP SWITCH	46EAA	RBSCB	RBSC	A
2 CKT BKR AUX PUMP	42FAB	LBSCC	LBSC	A
2 CKT BKR AUX PUMP	42FAB	RBSCC	RBSC	Α
2 CKT BKR	42FAB	RBSCC	OP	A
2 INFO ONLY, ENGINE FAILURE		вх	BX	FAAAAAAAA
2 COM/NAV IDENT		C		AAAAAAAA
2 COMMUNICATION		CA	C	F 00111112
2 FXTERNAL COMM ATTN		CAA	CA	111111111
2 REDUNDANCY ATTN		CAB	CAA	111111111
2 SECURE VOICE		CAD	CAA	00000000
2 CODER UNIT	69AA1	CADA	CAD	Α
2 MOUNT CODER	69AH1	CAUB	CAD	0
2 CONTROL UNIT	69AC1	CADC	CAD	A
2 RELAY	69AD1	CADD	CAD	A
2 CIRCUIT BREAKER	42FCD	CADE	CAD	8
2 UHF-AM COMM		CAE	CAH	111111111
2 RECEIVER-TRANSMITTER	63441	CAFA	CAE	8
2 CHASSIS ASSY	63AAA	CAFB	CAE	8
2 PREAMP-RF	63AAB	CAEC	CAE	8
2 AMPLIFIER-IF	63AAL	CAED	CAE	8 .
2 AMPLIFIER-IF	63AAD	CAEE	CAE	8
2 MODULATOR-AUDIO AMP	63AAE	CAEF	CAE	8
2 SPECTRUM GENERATOR	63AAF	CAEG	CAE	8
2 POWER AMPLIFIER XMITTH	63AAG	CAEH	CAE	3
2 RECEIVER-GUARD	63AAH	CAEJ	CAE	1
2 PWR SUPPLY	63AAJ	CAEK	CAF	8
2 MECHANICAL TUNER	63AAK	CAEL	CAF	8
2 INDICATOR SWR	63AB1	CAEM	CAF	0
2 BLOWER EXTERNAL	63AC1	CAEN	CAF	A
2 MOUNT-P/T	6.2 A D 1	Market Ma	CAE	2

CAEP

CAED

CAER

CAER

CAES

CAFT

CAF

CAF

CAFA

CAFB

CAFC

CAFD

CAFE

CAFF

CAFG

63AD1

63AF1

63AF1

63AF1

63AG1

42FCD

62AA1

62AAA

62AAH

62AAC

62AAE

62AAF

62AAG

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02

U2

02

172

02

02

112

112

71

72

MOUNT-R/T

ANTENNA

ANTENNA

DZ VHF-FM COMM

DZ VHF-FM COMM

IF AMP

CONTROL UNIT

FILTER-POWER

CHASSIS ASSY

RE OSCILLATOR

AUDIO AMP

CIRCUIT SREAKER

RECEIVER-THANSMITTER

AMTENUATOR VARIABLE

MODULATION AMP, XMITTER

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JUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUUU	1234567	3901234567	78901234567890123456	78901234567890
12 PWR SUPPLY	62AAH	CAFH	CAF	8
2 CONTROL UNIT-RF	LAASO	CAFJ	CAF	8
2 RF AMP #A6500<	62AAK	CAFK	CAF	8
2 RF AMP \$466004	62AAL	CAFL	CAF	8
2 OSCILLATOR BUFFER	62AAM	CAFM	CAF	8
2 VHF-TUNER	62AAN	CAFN	CAF	A
2 XTAL REF	62AAP	CAFP	CAF	8
2 GEAR BOX	62AAQ	CAFU	CAF	A
2 VOLTAGE REG	62AAR	CAFR	CAF	9
2 MOUNT R/T UNIT	62AP1	CAFS	CAF	J
2 CONTROL UNIT	62AC1	CAFT	CAF	8
2 SPIKE ANT	62AD1	CAFU	CAF	3
2 COUPLER ANT	62AE1	CAFV	CAF	8
2 FILTER-DC PWR	62AG1	CAFW	CAF	7
2 CIRCUIT BREAKER	42FCD	CAFX	CAF	8
2 VHF-AM COMM		CAG	CAB	111111111
2 RECEIVER/TRANSMITTER	62PA1	CAGA	CAG	8
CHASSIS ASSY	62RAA	CAGR	CAG	8
2 RECEIVER ASSY	62BAB	CAGC	CAG	3
EXCITER AMP. XMITTER	62BAC	CAGD	CAG	3
2 PWR SUPPLY	62BAD	CAGE	CAG	8
2 PWR CONTROL-SIDETONE	62BAE	CAGE	CAG	8
2 MODULATOR	62BAF	CAGG	CAG	3
2 PF AMP	62EAG	CAGH	CAG	8
Z MOUNT R/T	62881	CAGJ	CAG	Ö
2 CONTROL UNIT	62BC1	CAGK	CAG	8
2 POTENTIOMETER-SQUELCH	42FCG	CAGL	CAG	5
2 CIRCUIT BREAKER	42FCU	CAGM	CAG	8
2 COM/ICS	42100	CAH	CAA	AAAAAAAA
2 TRANSMIT CONTROL		CAJ	CAH	333333333
	64AAB	CAJA	CAJ	1
	644AB	CAJA	CAJ	8
24 MIC AMP 2 EA 64AAR		CAJB	CAJ	ì
	64ABB	CAJB	CAJ	8
24 TALK BUTTON CONT WHEEL	64AF1	CAJC	CAJ	1
26 TALK BUTTON-CONT WHEEL	64AF1	CAJC	CAJ	A
ZA FOOT SWITCH	64AG1	CAJD	CAJ	Ö
24 CORDAGE HEADSET PILOT	64401	CAJE	CAJ	ì
28 CORDAGE, HEADSET PILOT	64AD1	CAJE	CAJ	A
24 CORDAGE HEADSET COPILOT	64AEI	CAJE	CAJ	î
28 CURDAGE HEADSET COPILOT	64AEL	CAJF	CAJ	o
2 RECEIVER CONTROL	CTACL	CAK	CAH	111111111
2 RECEIVER CONTROL		CAK	CAM	AAAAAAAA
2A HEADSET AMP 2 FA 644BC	64AAC	CAKA	CAK	1
23 HEADSET AMP 64ABC		CAKA	CAK	8
2A HEADSET AMP 2 EA 64AAG	64ARC	CAKB	CAK	ì
	64ABC	CAKB	CAK	8
2 AUDIO POCESSING	DYANC	CAL	CAH	ΑΑΑΑΑΑΑΑ
		CAL	CAM	ΑΔΑΔΑΔΑΔΑ
2 UDID POCESSING	44441	CALA	CAL	1

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200	0000001111111111	22 22 22 22 22 3	111111	3344444444	445555555555666666	666677777777778
123	4567890123456789	01234567890	1234567	8901234567	390123456789012345	673901234567890
	CONTROL AIC-18		64AA1	CALA	CAL	8
024	CUNTROL AIC-25	ZEA 64AAL	64AR1	CALB	CAL	1
1128	CONTROL AIC-25	64441	64AB1	CALB	CAL	9
124	CHASSIS ASSY	2EA 54ABA	64AAA	CALC	CAL	1
023	CHASSIS ASSY	64ABA	64AAA	CALC	CAL	8
1124	CHASSIS ASSY	ZEA 64AAA	64ABA	CALD	CAL	1
	CHASSIS ASSY	64444	64ABA	CALD	CAL	8
112	TERM BLOCK		64AC1	CALE	CAL	0
0.2	RESISTORS		42FBF	CALF	CAL	1
02	CIPCUIT BREAKER		42FAB	CALG	CAL	A
.12	NAV/ICS CONTROL			CAM	CCD	F111111111
172	NAV/ICS CONTROL			CAM	CCM	AAAAAAAA
	IDENTIFICATION			СВ	C	00000000
1124				CHA	СВ	88888888
125	[FF			CRA	CB	AAAAAAA
02	R/T APX-64	65AC1	65 AA1	CBAA	CPA	3
12	R/T APX-72	65AA1	65AC1	CHAB	CBA	9
02	CHASSIS ASSY	65ACA	65AAA	CHAC	CBA	8
02	CHASSIS ASSY	05444	65ACA	CBAD	CBA	8
02	RE MODULE	65ACB	65AAB	CBAE	CBA	8
112	RE MODULE	65AAB	65ACB	CBAF	CBA	8
12	IF MODULE		65AAC	CBAG	CBA	8
02	DECODER MODULE		65AAD	CHAH	CBA	8
112	DELAY LINE MODU	ILE	OSAAE	CBAJ	CHA	8
112	CODER MODULE		65AAF	CBAK	CBA	8
02	KEF SIG GEN MOD	ULE	65AAG	CHAL	CRA	9
112	POWER SUPPLY MC		65AAJ	CBAM	CBA	8
02	TEST MODULE		65AAK	CHAN	CBA	0
1.2	MOUNT R/T APX-	-64	65AB1	CBAP	CRA	0
02	MODULATOR		65ACC	CBAO	CBA	8
112	DETECTOR		65ACD	CBAR	CRA	8
02	PRINTED CRKT CA	SE	SACE	CBAS	CBA	8
92	ENCODER CONT.		65ACF	CBAT	CBA	9
(12	ENCODER CLOCK		65ACG	CBAU	CHA	8
02	DECODER		65ACH	CBAV	CHA	8
02	PWR SUPPLY		65ACJ	CBAW	CBA	9
02	ENCODER GATING		65ACK	CHAX	CHA	3
02	MUDE 4 MODULE		65ACL	CBAZ	CBA	8
112	PROCESSOR		65ACM	CBAZA	CHA	8
0.2	XMTTR MODULE		65ACN	CRAZB	CBA	8
J2	PCVR MUDULE		65ACP	CBAZC	CBA	8
72	DELAY LINE		65ACQ	CBAZD	CBA	8
02	MOUNT R/T APX	-72	65AD1	CBAZE	CBA	C
72	CONTROL UNIT		65AF1	CBAZE	CBA	A
6.2	TEST SET XPND	R	65AF L	CHAZG	СВА	0
02	SIG GEN : REC		65AFA	CBAZH	CHA	0
112	FVALUATOR		65AFB	CRAZJ	CBA	8
02	TIMMING ASSY		65AFC	CRAZK	CBA	8
12	DIRECTIONAL CPL	R	65AFD	CRAZL	CHA	9
0.5	REGULATOR ASSY		65AFF	CBAZM	CBA	8

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007300000111111111112222222222				
02 CRKT CARD ASSY	65AFF	CHAZN	CRA	8
02 MOUNT TEST SET	65AG1	CBAZP	CHA	0
112 ANTENNA ZEACH	654H1	CHAZO	CBA	2
02 SW UNIT ANTENNA	65AM1	CHAZR	CBA	2
02 UHF HOLD RELAYMUNKNY	65AN1	CBAZS	CBA	0 .
OZ SW ANTENNA SEL	65AP1	CBAZT	CBA	2
02 IFF CAUTION LITE	65AQ1	CBAZU	CBA	0
02 CRYPTO COMPUTER	65BAL	CHAZV	CRA	1
02 MOUNT CRYPTO	65181	CBAZW	CBA	ō
02 CONNECTOR	658BA	CBAZX	CBA	1
02 WIRING	65BC1	CHAZY	CBA	i
02 CIRCUIT BREAKER 2 EA	42FCU	CBAZZ	CBA	8
02 TRANSMITTER MODULE	65AAH	CBAZZA	CBA	8
12ARADAR BEACON		CBB	CB	333333333
024 RECEIVER/XMTTR	72441	CBBA	CB3	8
OZA RE MODULE	72AAA	CRRB	CBB	8
024 IF AMP	72AAB	C38C	CBB	8
OZA ENCODER/DECODER	72AAC	CBBO	CBB	ä
024 MODULATOR	72AAD	CBBE	CH3	н
DZA PWR SUPPLY	72AAF	CBBF	CBS	3
JZA ANT ASSY	72AB1	CBBG	CBB	a
UZA CIRCUIT BREAKER	42+CD	СНВН	CBB	3
02 NAVIGATION		CC	C F	001111110
112 CLOCK	518AK	CCAA	cc	0
OZ HOUR METER	518AL	CCAB	cc	C
12 NAV. ALDS REDUN. ATTEN.	71000	CCB	cc	111111111
12 TACAN INFO		CCD	CCB	111111111
112 REC/XMTTR	71841	CCDA	000	8
12 CHASSIS ASSY	718AA	CCOB	CCD	8
DZ RF MUDULE	718AB	CCDC	CCO	8
12 ANT SEL MODULE	718AM	CCOD	CCD	2
12 PWR SUPPLY	71BAP	CCOF	CCD	8
12 MOUNT R/T	71861	CCOF	CCD	Ö
02 CONTROL UNIT	71801	CCOG	CCD	8
12 ANTENNA 2 FA	71PE1	CCDH	CCD	2
DZ FAN COOLING	718J1	CCDJ	CCD	Δ
02 CAPACITOR	42FCF	CCOK	CCD	8
12 CIRCUIT BREAKER 2 EA	42FCD	CCDL	CCD	8
UZ SWITCH-ANTENNA-UPP ELWR	71601	CCDM	CCD	8
12 CARLES & CONVECTORS	718F1	CCDN	CCD	5
DE TACAN RANGE		CCE	CCD	222222242
UZ RANGE DECODER	71BAC	CCEA	CCF	8
12 RANGE A MODULE	71 FAD	CCEB	CCE	3
12 RANGE B MODULE	716AF	CCEC	CCL	8
112 RANGE MECH MODULE	71FAF	CCED	CCE	3
12 AIR TO AIR MODULE	TIFAN	CCFE	CCF	ĭ
02 SOHI DISPLAY		CCF	CCF	ΑΛΛΑΛΑΑ
DZ HOHI INDICATOR	71861	CCFA	CCF	A
DE TACAN BEARING		ccc	(2)	99999949
OZ BEARING DECODER	71 PAG	CCGA	CCG	3

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0.0000000111111111122222222222	33333333	334444444	44455555555556666666 578901234567890123456	8901234567890
J2 BEARING A MODULE	718AH	CEGB	CCG	3
12 BEARING B MODULE	71PAJ	CCGC	CCG	8
12 BEARING MECH MODULE	7184K	CCGD	CCG	8
12 MAG PHASE DET AMP	71BAL	CCGE	CCG	8
2 SOHI DISPLAY		CCH	CCG	111111111
12 HOH! INDICATOR	71BG1	CCHA	ССН	<b>A</b>
12 COURSE INDICATOR DISPLAY		CCJ	CCH K CC	H 533333333
12 COURSE INDICATOR DISPLAY		CCJ	CCG	F111111111
OF CHURSE INDICATOR DISPLAY		CCJ	CCK	FAAAAAAAAA
12 COURSE INDICATOR	716H1	CCJA	CCJ	A
UZ CAPACITOR VERTICAL NEEDLE	42FBG	CCJB	CCJ	A
UZ VHF/FM BEARING		CCK	CCB	111111101
1.2 VHE HOMING MODULE	62AAD	CCKA	CCK	8
12 ANTENNA HOMING	62AF1	CCKB	CCK	н
02 SWITCH BEARING SEL	99624	CCKC	CCK	5
12 LF/ADF BEARING		CCM	CCB	111111111
02 SIGNAL PROCESSING		CCN	CCM	ΑΛΑΑΑΑΑΑ
112 RECVR	71441	CCNA	CCN	8
112 CHASSIS ASSY	71144	CCNH	CCN	8
02 FIRST RF AMP	71 AAB	CCNC	CCN	8
92 MODULATOR	71AAC	CCND	CCN	d
12 RF AMP	71AAD	CCNE	CCN	8
12 IF AMP	71AAF	CCNF	CCN	8
12 AUDIO AMP	71AAF	CCNG	CCN	9
02 MIXER	71 AAG	CCNH	CCN	8
UZ LUCAL USC	71AAH	CCNJ	CCN	8
12 BF MSC	71AAJ	CCNK	CCN	1
12 PWR SUPPLY	71 AAK	CCNL	CCN	8
G2 MOTOR GEAR CASE	71 AAL	CCNM	CCN	8
D2 RCVR MOUNT	71461	CCNN	CCN	0
112 PWR INVERTER	71ABA	CCNP	CCN	8
DE CONTROL UNIT	71AC1	CCNQ	CCN	8
DZ LUOP ANTENNA	71AD1	CCNR	CCN	H
UZ COMPENSATOR	71 ADA	CCNS	CCN	2
DE SENSE ANTENNA	71 AF1	CCNT	CCN	8
02 FILTER	71 AJ1	CCNU	CCN	4
02 CIRCUIT BREAKER	42FC0	CCNV	CCN	8
UZ HOHI DISPLAY		CCP	CCM	ΛΑΑΑΑΑΑΑ
32 BOHT INDICATOR	71861	CCPA	CCP	A
12 GYPO COMPASS INFO		CCO		W 11111111
12 COMPASS SIG PROCESS		CCR	cc 3	ΛΑΑΑΑΑΛΛ
124 DIR GYRO ASSY	51881	CCRA	CCR	В
JZA DIR GYRO	SIBHA	CCRH	CCF	3
SZA PWR SUP-AMP	>1888	CCRC	CCP	8
124 ELECT CONT AMP	SIRPC	CCRD	CCR	8
12A MAG DET	51886	CCRE	CCR	A
UZA COMPENSATOR	SILSE	CCRF	CCR	2
DEA ANNUNCIATOR BUKNS	SIEBF	CCRG	CCR	)
112 MAG FLUX DET	SIEAC	CCRH	CCR	Δ
"2 SLAVING IND	SICAH	CCBJ	CCR	0

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1234567890123456789012345678901		CCRK	CCA	343313	8
C25 DIRECTIONAL IND VAC *GYRGC			CCR		8
DEA DIRECTIONAL IND #GYROK	STEAD	CCRL			
OZ COMPASS DISPLAY		CCS	CCO		
12A3DHI DISPLAY		CCT	CCS		
HERADHI DISPLAY	71061		CCS		111111111
JE BOHT INDICATOR	71861	CCTA	000		3
DESHEADING IND DISPLAY		CCU	CCS		A
026 DIR IND 02 HEADING	SIBAG	CCV	CCU		001000110
		CCM	CCV	K CCO	AAAAAAAAA
02 STANDBY HEADING	510A1	CCWA	CCW	r ccs	3
02 STANDBY COMPASS 02 INFORMATION AND DISPLAY	51BAJ	D	CCN		ΑΑΑΑΑΑΑΑ
02 FLIGHT STATUS		DA	D		011111130
02 OUTSIDE AIRTEMP		DB	DA		000000000
02 OAT INDICATOR	SIEAC	DBA	DR		8
	STEAC	DC	DA	Ε	004111440
J2 ALTITUDE INDICATION		00	CBA	C.	111111111
02 BAROMETRIC ALTITUDE		20	DC		AAAAAAAA
	SICAR	DDA	00		8
112 ALTIMETER SICAK	SICAB .	008	00		8
UZ ALTIMETER AAU-21 51CAH	SICAK	DE	DC		000000000
12 VERTICAL VELOCITY INDICATIO		DEA	DE		8
	51 CAA	OF	DA		
12 ATTENUATION		OG OG	DF		000010000
D24 G-LOAD INDICATION	ELCAC	DGA	DG		8
MIZA ACCELEROMETER	51CAG	DH	DE		051010150
02 AIRSPEED INDICATION	E1044	DHA	DH		8
02 AIRSPED INDICATOR 02 STATIC SOURCE	51BAA	DJ	DC		SAAAAAAAA
G2 STATIC SOURCE		07	20		FAAAAAAAAA
22 STATIC SOURCE		DJ	DE		FAAAAAAAAA
DZ STATIC SOURCE		DJ	DH		ΑΑΑΑΑΑΑΑ
DE VALVE SOURCE SELECT	SIDAR	DJA	DJ		0
OZ BUTTON STATIC SOURCE #2FA		DJB	DJ		1
DZ PITOT SENSE	COLUMN	DK	DH		44444444
02 PITOT TUBE	51 DAA	DKA	DK		8
02 PITOT HEAT	SIUMA	DL	DK	A	AAAAAAAA
UZ PITOT HEAT		DL	DV	Δ	4444444
02 SWITCH PITOT/STALL HEAT	SIDAF	DLA	DL		A
02 CKT BKR	42FAB	DLB	DL		Ä
02 ATTITUDE	721 40	DM	DA	E	CA1111140
DE PITCH/ROLL INDICATION		DN	DM	DP	111111111
OZA ATT IND ELECTRIC	SICAE	DNA	DN	Ů.	8
1128 ATT IND VACUUM	SICAF	DNA	DN		8
12 TURN/SLIP INDICATION	J.C.	DP	DM	K DN	ΑΑΑΑΑΑΑΑ
DZ INDICATOR	SICAC	DPA	OP		8
324 ELECTRIC DRIVE	2.10.110	00	DN		
024 CKT BKR	42FAB	DUA	00		Α
UZE VACUUM OFIVE	121 40	DR	CCS		4444444
DZB VACUUM DRIVE		OR	DN		ΑΑΑΑΑΑΑΑ
UZH GAGE SUCTION	51444	DRA	DR		3
UZU GAUL SUCTION		V.4			

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000000000111111111122222222222	3333333	833444444	44445555555555566 6789012345678901	66666666	77777777778
026 FILTER VACUUM	SIAAC	DRB	DR		1
123 MANIFOLD	SIAAG	DRC	DR		i
023 FRUNT VACUUM SOURCE		LOS	DR	KRDS	AAAAAAAA
DEB REAR VACUUM SOURCE		RDS	DR	KLDS	AAAAAAAA
123 VACUUM PUMP	SLAAD	LDSA	LOS		Δ
123 VACUUM PUMP	SIAAC	RDSA	RDS		Δ
1129 RELIEF VALVE	STAAF	LDSB	LOS		1
028 RELIEF VALVE	51AAE	RDSB	RDS		1
123 CHECK VALVE	SIAAF	LDSC	LDS		ī
124 CHECK VALVE	SLAAF	RDSC	PDS		1
OZE OIL SEPERATOR	SIAAB	LDSD	LDS		1
02" OIL SEPERATOR	SIAAB	ROSD	POS		ī
D2 WARNINGS	2	DT	0		ΑΑΑΑΑΑΑΑ
02 ENGINE FIRE WARNING		DU	DT	x	AAAAAAAA
12 DETECTORS 4 EA	49844	DUA	DU		1
32 WIRING	49BAC	DUB	0U		Ā
02 FIRE DET WARN LIGHT	99491	DUC	DU		4
02 STALL WARNING	,,,,,,,	DV	10		000000000
12 DUAL WARN UNIT	SIEAA	DVA	DV		8
02 DUAL WARNING UNIT	SIEAA	DVA	NU		1
02 ACTUATOR STALL WARN	SIEAB	DVB	DV		Ā
22 TRANSISTOR	42FHC	DVC	DV		A
2 AMP ASSY AURAL WARN	42FBD	DVD	DV		8
112 AMPLIFIER ASSY AURAL WNG	42FBD	OVD	NU		1
02 DIDDE	42 FBE	DVE	DV		Ā
02 CKT BKR	42+AB	DVF	ÇV		A
DZ ENVIRONMENTAL CONTROL	12.110	E			AAAAAAAA
12 LIGHTING		EA	F	D	111111121
12 INTERNAL LIGHTING		EAA	EA		011111110
DZ NORMAL LIGHTING		EAB	EAA	EAF	111111111
12 FLIGHT INSTRUMENTS		EAC	EAR		22222222
12 INSTRUMENT LIGHT SYSTEM	44AD1	EACA	EAC		1
12 RHEOSTAT	44AE1	EACB	EAC		5
12 CKT BKR	42FAB	EAGC	EAC		A
12 ENGINE INSTRUMENTS		EAD	EAB		111111111
CZ INST LIGHT SYS	44AD1	EADA	EAD		1
02 RHEOSTAT	44AE1	EADB	EAD		5
UZ CKT BKR	42FAB	FADC	FAD		4
UZ CKT BKR	42FAB	EADC	EAG		Δ
22 SHITCH/CONTROL PANEL		EAE	EAR		000000000
TE INTERIOR LIGHT SYSTEM	444(1	EAEA	EAE		1
02 RHEOSTAT	44At1	EAEB	EAF		5
GE BACKUP LIGHTING		EAF	EAA	K EAB	ΑΑΑΑΑΑΑΑ
UZ DOME LIGHTING		EAG	EAF		111111111
G2 INTERIOR LIGHT SYSTEM	44AC I	EAGA	EAG		1
UZ CKT BKR	42FAB	EAGB	EAG		i
DZA CKT BKP	42FAB	EAGB	EAH		<u> </u>
DE UTILITY/MAP		EAH	FAF		111111111
CZA INTERIOR LIGHT SYS 2 EA	44AC1	EAHA	EAH		1
028 INTEPIOR LIGHT SYSTEM	44AC1	EAHA	EAH		4

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	00000 <b>01111111111222222222223</b> 3					
1121	RHEOSTAT	44At 1	FAHC	EA		5
028	RHEDSTAT	44AE1	EAHC	FA		5
	INSTRUMENT FLOOD	*****	EAJ	FA		111111111
028	INTERIOR LIGHT SYSTEM	44AC1	EAJA	FA		1
120	CKT BKR	42FAB	FAJB	EA		A
1)2A	CKT BKR	42FAB	EAJB	EA		Ā
02	EXTERNAL LIGHTING		EAK	EA		111111111
12	ATTENUATION		EAL	EA		111111111
02	ANTI COLLISION		EAM	EA		000000000
112	ANTI COLLISION LIGHT	44444	EAMA	EA		A
112	CKT BKR	42FAB	EAMB	EA		A
92	LANDING		EAN	FA		00000010
02	LANDING LIGHT SYSTEM \$2EAG	44481	EANA	FA		1
32	CKT BKR	42FAB	FANC	FA		A
02	TAXI		EAP	EA		200000000
02	LAND LIGHT SYSETAXIC 2 EA	44AB1	EAPA	EA		5
172	CKT BKR	42FAB	EAPC	FA	P	A
1.2	NAVIGATION		EAQ	FA		600600000
02	NAV LIGHT SYS	44AA1	EAUA	FA		2
0.2	CKT BKR	42FAB	EAQB	EA		A
72	CABIN ENVIRONMENT		EB	E		111111111
02	WINSHIELD CLEAR		EBA	FA	Y	013000030
0.5	DEFROSTER CONTROL	41 DAC	EBAA	C B	A	A
02	PILOTS DEFROST		LEBB	ER	A KREBB	AAAAAAAA
112	COPILOTS DEFROST		REBB	FB	A KLEBR	AAAAAAAA
0.2	VALVE	41CAA	LEBRA	LEB	IR .	3
02	VALVE	41CAA	REBBA	REB	18	3
0.2	DUCT	41CAB	LEBBB	LFH	8	1
.)2	DUCT	41 CAB	REBBB	REB	18	1
.12	OUTLET UNION	41CAC	LEBBC	LFR	8	1
0.5	OUTLET UNION	41CAC	REBBC	REA	В	1
35	CABIN HEATED		EHC	F8		000000000
62	PILOT AIR MIXING		LEHD	LEB	В	ΑΑΑΑΑΑΑΑ
12	PILOT AIR MIXING		LEBO	EB	C	111111111
0.2	COPILOT AIR MIXING		REBO	KER	B	AAAAAAAA
1,5	COPILOT AIR MIXING		READ	EB		111111111
115	AIRBOX	41AAA	LEBDA	LEB		1
115	ATRBOX	4LAAA	REBUA	RER		l
12	HAFFLE	41448	LEBOR	LFB		
02	HAFFLE	41AAB	REBDB	REB		
r12	VALVE	41AAC	LEBUC	LEB		Я
112	VALVE	41 AAC	REBDC	REA		8
112	VENT BOX	41AAD	FERDD	LEH		1
0.2	VENT BOX	41AAD	REBUD	REB		
()2	AIR DUCT	41 AAE	LEBDE	LEB		
(12	AIR DUCT	41 AAE	REBDE	REP		1
12	CABIN HEAT CONTRUL	41LAB	LEBDE	LER		8
02	CABIN HEAT CONTROL	410AB	REBOF	REB		8
0.2	EXHAUST MUFFLER	CINAD	LEBDG	LEA		8
115	EXHAUST MUFFLER	SINAD	REROG	REB	U	8

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200	455789012345678901234567890	The second secon			
12	SHROUD	21NAE	LEBDH	LEBD	End of the Williams
0.5	SHRUUD	ZINAF	REBOH	REBD	
02	CABIN HEAT	41UAA	LEBDJ	LEBD	8
1.2	CABIN HEAT	410AA	REHDJ	REBO	8
12	VENTILATION		FRE	EB	000000000
12	VENT-AIR 2 FA	41844	EREA	ERE	2
12	AI) APTER	41BAB	FBEB	FBF	
.5	CONTROL CABIN AIR 2 EA	41DAB	EBEC	FRE	5
12	AIR SCOOP	41BAC	EHED	ERE	
120	PLENUM	41BAD	EBEE	FRE	
15	SHUTOFF VALVE	41BAE	EBEF	EBE	1 200
12	INLET ASSY 2EA	41BAF	EBEG	ERF	3
15	DUCT 2 EA	418AG	EBEH	EBF	Teach I was to do not
15	CABIN HEAT	41DAA	EREJ	EBE	5
12	FLIGHT CONTROL		F		AAAAAAAA
. 7.	LIFT AUGMENTATION		FA	F C	010000030
12	FLAPS POSITIONED		FAA	FA	ΑΛΑΛΛΑΔΑ
12	LEFT FLAPS POSITIONED		LFAG	FAA	ΛΑΑΛΛΑΔΑ
15	RIGHT FLAPS POSITIONED		KFAB	FAA	ΑΑΑΑΑΑΑ
12	RIGHT FLAPS POSITIONED		REAB	FCH	FAAAAAAAA
5	CABLE	14DAK	LFABA	LFAB	A
?	CABLE	14DAK	REARA	RFAS	A
2	PULLEYS	14DAL	LFABB	LFAB	9
2	PULLEYS	140 AL	REARR	REAR	8
2	QUADRANT AND BELLCRANK	140 AR	LFARC.	LFAB	7
2	QUADRANT AND BELLCHANK	140AR	REABC	REAB	7
2	BELLCRANK	14CAS	LFABD	LFAB	3
2	BELLCRANK	14DAS	RFABD	REAB	3
2	OUT BOAPD FLAPS POSITIONED		LFAC	LFA9	666666666
2	CUTBOARD FLAPS POSITIONED		RFAC	REAR	660666666
2	FLAP, DUTBO	14048	LFACA	LFAC	3
2	FLAP, OUTBD	14DAB	RFACA	RFAC	3
2	LINKS 2 EA	14DAM	LFACE	LFAC	5
12	LINKS 2 EA	140AM	REACB	KFAC	5
2	ROO	140AT	LFACC	I FAC	5
2	RID	140AT	RFACC	RFAC	5
2	PANEL FLAP GAP	14LAC	LFACD	LFAC	0
12	PANEL FLAP GAP	14LAC	REACD	RFAC	0
2	INBOARD FLAPS POSITIONED		LFAD	LFAR	44444444
12	INBOARD FLAPS POSITIONED		READ	REAB	44444444
2	FLAP INHOARD	14044	LFADA	LFAD	3
2	FLAP INBOARD	14DAA	READA	RFAD	3
1	LINK	14DAM	LEADP	LFAD	Δ
2	LINK	140AM	READH	PFAD	4
12	PANEL FLAP GAP	14DAC	LFADC	LFAD	0
2	PANEL FLAP GAP	14UAC	READC	RFAD	3
.2	FLAP DRIVE		FAE	FA	ΔΑΑΑΑΑΑ
2	FLAP MOTOR	14DAN	FAFA	FAE	٨
12	ACTUATOR	14DAQ	FAEB	FAE	8
12	CKI SKR	42FAR	FAFC	EAF	٨

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000	000000111111111122222222223 +567890123 <b>45</b> 678901234567890	3333333	33444444	4444555555555566	666666667	777777778
0.2	FLAP CONTROL	1234301	FAF	FAE	2343010301	ΑΑΑΛΑΑΛΛ
17.2	CONTROL LEVER	14040	FAFA	FAF	R	<b>ччними</b>
02	SWITCH FLAP OPERATING	140AE	FAFB	FAF	7	
112	CONTROL FOLLOW UP	140AG	FAFC	FAF	i	
12	POINTER POSITION	14DAF	FAFD	FAF	ó	
12	LIMIT SWITCHES 2 EA	140AH	FAFE	FAF	3	
12	YAW CONTROL	THUAR	FB	F	,	CAAAAAAA
02	RUDDERS POSITIONED		FBA	FB		010000030
50	LEFT RUDDER POSITIONED		LF86	FbA		22222222
62	LEFT RUDDER POSITIONED		LFBB	FRA	KREBB	AAAAAAAA
22	RIGHT RUDDER POSITIONED		REBB	FRA	KKLDD	22222222
02	RIGHT RUDDER POSITIONED		REBB	FBA	KLERR	AAAAAAAA
02	RUDDER ASSY	14CAE	LEBRA	LFAB	3	<b>А</b> ВАВАВАВ
0.5	RUDDER ASSY	14CAE	REBBA	REBB	3	
02	BALANCE WEIGHT	14CAF	LFBBB	LEBB	ő	
02	BALANCE WEIGHT	14CAF	REBBB	RFBB	0	
02	RUDDER HINGE ASSY	11688	LFBBC	LFBB	2	
02	RUDDER HINGE ASSY	11688	REABC	REBB	2	
02	RUDDER CONTROL	11000	FBC	FBA	2	AAAAAAAA
02		14048	FBCA	FBC	A	дададада
	BELLCRANK	Ten College College		FBC		
02	CABLES	14CAL	FRCR		A	
	PULLEY	14CCA	FRCC	FBC FBC	8	
02		14008	FBCD	FAC	7	
0.2	BELLCRANK 2 EA	14000	FRCE			001111100
02	PUDDER PEDAL CONTROL	14.46	FBD	FRC		091111190
02	PEDAL SUPPORT 2 EA	14CAC	FBDA FBDB	FBD FBD	1	
112	RUDDER PEDAL 2 EA	14CAA	FRE	FBC		111111111
02		14604	FREA	FRE	8	IIIIIIII
	WHEFL ASSY	14CDA		FBE		
02	TRIM INDICATOR	14008	FBEC	FBE	O A	
_	CHAIN	14CDD			A	
02	SPROCKET ACTUATOR	14CDE 14CDH	FBFD	FBE	7	
12	HUNGEE	13644	FBEF	FBE	7	
	PITCH CONTROL	13644	FC.	F		
12	ELEVATOR POSITIONED		FCA	FC		
72	ELEVATOR POSTTIONED	14844	FCAA	FCA	,	<b>ААЛАДАДА</b>
02	ARM AND BALANCE WEIGHT	14848	FCAB	FCA	3	
112	FLEVATOR HINGE ASSY	11GAB	FCAC	FCA	3	
02	ELEVATOR DRIVE/CONTROL	IIGAN	FCB	FCA		031111100
112	CABLE	14004	FCBA	FCB	A	031111195
02		1488A	the same of the same			
	PULLFY	14888	FCBB	FCB	8	
12	BELLCRANK	1488C	FCBC	FCB	A	
112	PILOT CONTROL	1488D	FCBD	FCH FCH	K FCD	AAAAAAAA
02	CONTROL WHEEL	14FAA	FCCA	FCC		<b>АДАДАДА</b>
72	BEARING	14FAB	FCCB	FCC	1	
02	CONTROL COLUMN ASSY	14FAC	FCCC	FCC	6 A	
720	HUB WEIGHT	14FAF	FCCD	FCC	3	
02	COPILOT CONTROL	TALMA	FCD	FCR	K FCC	AAAAAAAA
	C. IL. C. TINGE		160	, 6,17	" " "	MAMMAN MAN

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FLIGHT SAFETY PREDICTION TECHNIQUE

	000000111111111112222222222 45678901234567890123456789					
02	CONTROL WHEEL	14544	FCDA	FCD	234301070	1234201090
02	HE AR ING	14548	FCOR	FCD		
112	CONTROL COLUMN ASSY	14FAC	FCDC	FCD		
023	BUB WEIGHT	14FAF	FCDD	FCD		
02	TRIM TAB POSITIONED	TTIA	FCE	FCA	K FCB	AAAAAAAA
112	TRIM TAB	14BAC	FCEA	FCE	~ 100	
02	INDICATOR	14808	FCEB	FCE		
112	TRIM ACTUATOR	148CH	FCEC	FCE		
0.5	STUP BLOCK	14BCL	FCED	FCE		
(12	CHAIN	14800	FCEF	FCE		
02	PULLEY	148CG	FCFF	FCE		
72	CAULE	14FCE	FCEG	FCE		
	MANUAL TRIM	141.00	FCF	FCE	FCG	111111111
	MANUAL TRIM		FCF	FCF	,,,	AAAAAAAA
1)2	TRIM CONTROL WHEEL	14HCA	FCFA	FCF		
02	SPRUCKET	148CC	FCFR	FCF		
	ELECTRIC TRIM	14000	FCG	FCF	FCF	111111111
021		148CJ	FCGA	FCG	10,	
024	ELECTRIC TRIM DRIVE	14BCK	FCGB	FCG		
024		42FAB	FCGC	FCG	7	
02	FLAPS/ELEVATOR INTERCONNECT	and the same of th	FCH	FCF		010000000
02	INTECONNECT CABLE ASSY	14DAU	FCHA	FCH		
112	ROLL CONTROL	14040	FD	F		CAAAAAAO
12	AILERONS POSITIONED		FDA	FD		AAAAAAAA
12	LEFT AILERON POSITIONED		LFOB	FDA		222222222
112	LEFT AILERON POSITIONED		LFDB	FOA	KREDB	AAAAAAAA
112	RIGHT AILERON POSITIONED		REDB	FDA	KALOD	22222222
112	PIGHT AILERON POSITIONED		REDB	FDA	KLEDB	AAAAAAAA
u2	ALLERON	14000	LEDBA	L FDB	3	
32	ALLERON	14444	REDBA	REDR	3	
112	HALANCE WEIGHT	14AAB	LFDBB	LFD8		
02	BALANCE WEIGHT	14048	SEDBB	REDR		
112	TRIM TAB	14AAC	LEDRC	LFDB	č	
112	TPIS TAB	14AAC	REDBC	REDB	d	
02	RCD	14A4G	LEDBD	LFDB		
112	800	14AAG	REDBD	SEDB		
12	ALLERON CONTROL	14440	FDC	FDA		AAAAAAAA
112	PULLEY	14AAE	FOCA	FUC		10.11
112	BELLCRANK 2 EA	14AAF	FDCB	FDC		
112	CABLE	14AAH	FOCC	FDC		
92	PILOT CONTROL	LYAMIT	FUD	FDC	K FDE	AAAAAAAA
112	CONTROL WHEEL	14FAA	FUDA	FDD	1 102	
12	BEARING	14FAH	FDDB	FDD	6	
112	CONTROL COLUMN ASSY	14FAC	FDDC	FUO		
112	COPILOT CONTROL		FDE	FOC	K FOD	AAAAAAAA
112	CONTROL WHEEL	14FAA	FDEA	FDF	1	
52	BEARING	14FAB	FDEB	FDE	6	
02	CONTROL COLUMN ASSY	14FAC	FDEC	FDE	Δ.	
1)2	GROUND CONTROL	•	G			4444444
112	SPEED CONTROL		GA	G	c	00000000
	a cer continue		-	•	•	30000040

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cons	0000011111111112	222222223	3333333	33444444	44455555555556	6666666	777777778
1234	5678901234567890	1234567890	1234567	893123456	789012345678901	23456789	01234567890
02	SPEED CONTROL			GA	GAX		5000000005
0.5	ATTENUATION			GAX	G		111111111
02	DIRECTIONAL CONTE	ROL		GB	G		110000011
12	WHEFL BRAKES			GC	GA		ΑΑΛΑΑΑΑΑ
02	WHEEL BRAKES			GC	GB	K GG	AAAAAAAA
12	MASTER CYLINDER	2 EACH	13FAD	GCA	GC		8
12	WHEEL CYLINDER	2 SETS	13FAE	GCB	CC		8
2	PRESSURE PLATE	2 SETS	13FAG	GCC	GC		1
12	BACK PLATE	2 SETS	13FAH	GCD	GC		1
2	LINING	2 SETS	13FAJ	GCE	GC		1
2	TURQUE PLATE	2 SETS	13FAK	GCF	GC		A
2	DISC	2 SETS	13FAL	GCG	GC		1
2	TUBING	2 SETS	13FAM	GCH	GC		8
12	HOSE	2 SETS	13FAN	GCJ	GC		8
12	PARKING BRAKE			GO	GC		000000000
12	CONTROL ASSY		13+ AA	GDA	GD		8
2	PARKING BRAKE VA	ALVE	13FAC	GDB	GD		A
12	PILOT ACTUATION			GE	GC	GF	111111111
12	BRAKE PEDAL LIM	VK	13FAB	GEA	GE		Α
2	RUDDER/BRAKE PEL		14CAA	GEB	GE		Δ
2	PEDAL SUPPORT		14CAC	GEC	GF		4
2	COPILOT ACTUATION	4		GF	GC	K GE	AAAAAAAA
2	BRAKE PEDAL LINE		13FAB	GFA	GF		A
2	RUDDER/BRAKE PER		14CAA	GEB	GF		A
2	PEDAL SUPPORT		14CAC	GFC	GF		A
2	NOSE WHEEL STEER	ING		GG	GB	GC	111111111
2	BUNGEE		13GAA	GGA	GG		Α
2	STEERING CAM		13GAB	668	GG		A
2	BELL CRANK		13640	GGC	GG		Δ
2	LOCK		13GAD	GGD	GG		0
2	ROD		13GAE	GGE	GG		٨
2	STEERING COLLAR		13CAE	GGF	GG		Δ
2	TORQUE LINK		13CAF	GGG	GG		Ä
2	RUDDER BARLINK/RO	V22A OC	14CAD	GGH	GG		8
	SHIMMY DAMPENER	10 A331	13083	GGJ	GC		3
2	PILOT CONTROL		13003	LGH	GG	RGH	111111111
-	COPILOT CONTROL			RGH	GG	KLGH	ΑΛΛΑΑΛΛΑΑ
2	RUDDER/BRAKE PO	ENAL	14044	LGHA	L GH	KLIIII	A
	RUDDER/BRAKE PE		14044	RGHA	RGH		A
2	The same and survey and survey and the same	EDAL			LGH		A
-	PEDAL SUPPORT		14CAC	LGHB	RGH		A
2	PEDAL SUPPORT		14CAC	RGHB	КОП		**
2	MISSION SUPPORT	. •		M			AAAAAAAA
	OFFENSIVE ARMAMEN			MA	M		020010020
	SUSPENSION/RELEAS			MAA	MA		111111111
	STORES SUSPENSION		75.400	MAB	MAN		, 111111111
21	PYLON ASSY, INBO	J AZLAC	75480	MABA	MAB		1
ASI	SHELL MEEAK		75ABA	MARR	MAP		0
IZA	FAIRING \$2FA		75ABC	MARC	MAR		2
450	FAIRING \$2EAC		75AHD	MARD	MAB		0
12.4	SWAY BRACE ASSY	*ZEA<	75AHE	MARE	MAB		I state of the sta

PGG	195.J1R1 DATE = 01/12/76		FL	ICHT SAFETY PR	FUICTION TECHNIOU
000	200000111111111122222222233	121222	33444444444455	55555555666666	66661777177778
	56789012345678901234567890				
72A	RACK . BOMBSMA-44 %ZEA4	75 AB J	MABE	MAB	1
024	PYLON ASSY OUTBO KZEAC	75 AC G	MABG	MAH	i
1124	SHELL \$2EAC	15ACA	MAHH	MAB	o o
1121	FAIRING \$2FAC	75ACC	MABJ	MAR	0
12A	FAIRING #2EAC	75ACD	MABK	MAH	0
1121	SWAY BRACE ASSY #2FAC	75ACE	MARL	MAB	1
024	RACK BOMB SMA-44 \$2F44	75ACJ	MABM	MAR	1
024	GUNS		MAC	MAB	111111111
024	MACHINE GUN POD SUU-11A	75CAC	MACA	MAC	1
024	MACHINEGUN ASSY	75CAA	MACB	MAC	1
057	SWITCH-GUN BATT CHARGE	75BAB	MACC	MAC	0
02A	CKT BKR GUN BATT CHARGE	42FAB	MAGD	MAC	C
1124	BOMBS/ROCKETS/MISSLES		MAD	MAR	111111111
024	DISPENSER, BOMBRACK \$4EAC	75CF0	MADA	DAM	1
024	SWAY BRACE ASSY #4EAC	75CFA	MADB	MAD	0
450	SHELL ASSY #4EAC	75CFC	MADC	MAD	0
UZA	HUMB RACK *MA-4< #4FA	75CFD	MADD	MAD	1
024	LAUNCHER ROCKET LAU-59	75CGC	MADE	MAD	1
112 A	LAUNCHER ROCKET LAU-58	75 CHO	MADE	CAM	1
124	BOMH DISPENSER COU-14	75CJ0	MADG	MAD	1
724	SWITCH PYLON RACK	75ARG	MADH	MAI	0
JSA	SWITCH PYLON RACK	75ACG	LUAM	MAD	0
	ARMAMENT CONTROL		MAE	MAA	111111111
	ARMING		MAF	MAE	_ 000000000
154	HANDLE ASSY ARMING \$2EAC	75ABF	MAFA	MAF	2
024	SOLENOID ARMING \$4FA	75 ARK	MAFB	MAF	1
024	LEVER COCKING #26A	75A3L	MAFC	MAF	2
124	HANDLE ASSY ARMING \$2EAC	75ACF	MAFD	MAF	2
024	SOLENOID ARMING %4FA	75ACK	MAFE	MAF	1
124	LEVER COCKING *2EA<	75ACL	MAFF	MAF	2
1124	SALVO ARM-RELEASE RELAY	75BAE	MAFG	MAF	٨
024	MASTER ARMAMENT SWITCH	758AF	MAFH MAFJ	MAF MAF	A
UZA DZA	CKT BKP BLOAK ARMING CKTS		MAFK	MAF	A
ASD	NURMAL RELEASE/FIRE	42146	MAG		MAH 111111111
ASC	MASTER ARMAMENT SWITCH	75BAE	MAGA	MAG	MAH 111111111
024	FIRE POROP RELAY \$2644	75AAA	MAGB	MAG	5
OZA	FIRE/DROP SWITCH %4EAC	75RAC	MAGC	MAG	2
C2A	CKT HKR #2044 #2E44	42FAB	MAGD	MAG	5
MSA	TRIGGER SWITCH	75AAD	MAGE	MAG	A
1,24	PANEL ELECTPOLUMINSENT	758AH	MAGE	MAG	ö
72A	POWER SUPPLY-PANEL	758AJ	MAGG	MAG	Š
02A	DIODERZEAS	75AAL	MACH	MAG	ì
1124	SOVAT SWITCH	13000	MAGJ	MAG.	5
1)21	CKT SKR #3AC GRD DISABLE	42FAH	MAGK	MAG	Å
1124			MAH		4AG
124	SALVO-ARM RELEASE HELAY	75AAB	MAHA	MAH	4
1124	JETTISON SWITCH	75140	MAHS	MAH	Ā
	AIMING		MAJ	MA	00000000
1124	GUNSIGHT ASSY	74141	MAJA	MAJ	9

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1234	000J0011111111112222222222345678901234567890	3333333	334444444444455555 89012345678901234	55556666666666666666666666666666666666	67777777778
OZA	RHEDSTAT	74AAD	MAJR	LAM	8
MSA	CKT BKR GUNSIGHT	42FAB	MAJC	MAJ	Δ
132A	PHOTO/RECON		MB	M	000000000
MSE	CAMERA ASSY KB-18	77444	MBA	MB	8
024	CONTROL	77AAE	MBR	MB	8
1124	CKT BKR CAMERA "3AK	42FAB	MBC	MR	4
024	SMOKE GENERATION		MC	М	000000000
UZA	TANK ASSY	95AAA	MCA	MC	1
721	PUMP-FUEL	95AAD	MCB	MC	A
1124	VALVE-SOLENOID	95AAE	MCC	MC	Δ
1121	SWITCH OFF-ON	9995A	MCD	MC	A
DZA	CKT BKR-SMOKE PUMP%3AC	42FAB	MCE	MC	Δ
026	PSYCHOLOGICAL WARFARE		MD	M	000000000
028	LOUDSPEAKER	69BA1	MDA	MD	8
023	DRIVE UNIT	69EAA	MDB	MD	8
023	AMPLIFIEP %3EA<	698E1	MDC	MD	5
028	CONTROL UNIT	698F1	MDD	MD	9
023	DISTRIBUTION PANEL	698G1	MDE	MO	8
728	RECORDER UNIT	69BH1	MDF	MD	5
1129	CKT BKR	42FCD	MDG	MD	A
1128	ELECT DISABLE CONTACTOR	9942C	MDH	MD	A
02	LANDING GEAR		N		ΑΑΑΑΑΑΑΑ
02	EXTEND GEAR		NA	N	000000040
02	ROLLING SUPPORT		NB	N	1800000A1
112	AXLE MAIN GEAR	136AC	NBA	NB	A
112	AXLE TUPE NOSE GEAR	13CAH	NBB	NB	A
J2	WHEEL ZEA MAIN	13EAA	NBC	NB	2
72	BEARING ZEA MAIN	13EAB	NBD	NB	6
112	TIRE 2 EA MAIN	13EAC	NBE	NB	1
02	TUBE 2 FA MAIN	13 EAD	NBF	NB	1
02	WHEEL NOSE	13FBA	NBG	NB	2
02	BEARING NOSE	13E88	NBH	NB	1
0.2	TIRE NOSE	13EBC	NBJ	NB	1
72	TUBE NOSE	13EBD	NBK	NB	1
112	SPRING STRUT ZEA MAIN	13848	NBL	NB	٨
72	SHOCK STRUT NOSE	13CAA	NBM	NB	A
112	TRUNNION NOSE	13CAB	NBN	NR	0
02	CYLINDER-SHUCK STRUT NOSE	13CAC	NBP	NB	1
1)2	PISTON-SHOCK STPUT NOSE	13CAD	NHO	NR	0
02	FIRK NOSE	13CAK	NBR	NP	Δ
112	PRESSURE DISTRIBUTION		NC	NA	ΑΑΑΑΑΑΑΑ
02	PRESSURE DISTRIBUTION		NC	ND	ΛΑΑΑΑΑΑΑ
0.2	POWER PACK	13A6A	NCA	NC	8
1)2	MANIFOLD	13ABB	NCB	NC	A
02	LOCKOUT SOLENDID	13ACA	NCC	NC	1
12	ACTUATOR MAIN GEAR	13BBA	NCD	NC	8
1)2	ACTUATOR HOSE GEAR	13CBA	NCE	NC	8
02	HOSE LA MH GR WHL DR CLOS		NCF	NC	1
1.5	HOSE LH MN GR WHL DR OPEN	13FBG	NCG	NC	1
.12	HOSE RH MY GR WHL DR CLOS	E1368H	NCH	NC	1 10 10 10 10 10

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	00000011111111112222222222333333333				
	45678901234567890123456789012345678	NCJ	NC NC	.5450154	1
02	HOSE RM MN GR WHL DR OPEN 1368J HOSE NOSE GR DR ACT OPEN 13CBK	NCK	NC NC		
35	HOSE NOSE GR DR ACT OPEN 13CBK	NCL	NC NC		
		NCM	NC NC		8
415	ACTUATOR-MN GR DOORS 13DCA ACTUATOR-NOSE GR POORS 13DCB	NCN	NC NC		8
32		NCP	NC NC		8
02	ACTUATOR-MN GEAR STRUT DR 13DCC RETRACT GEAR	NO	N		000000000
112	MAIN GEAR AND DUORS DOWN	NE	NA NA		AAAAAAAA
05	SAUDLE 2EA 13FAA	NEA	NE NE		2
112	DOWNLOCK ZEA 13BAD	NEC	NE NE		A
.12	DUWNLICK ADJ SUPPORT 2FA 13HAF	NED	NE		8
113	UPLOCK HOOK ZEA 138AJ	NEE	NE		1
132	U JOINT ASSY 2EA 13FAL	NEF	NE		i
52	LINKAGE ZEA 136AM	NEG	NE NE		
15	DOUR ASSY 2EA 13DAA	NEH	NE NE		o
02	DOOR ASSY STRT ZEA 13DAB	NEJ	NE NE		C
02	MOSE GEAR AND DOORS DOWN	NE	NA		AAAAAAAA
02	UPLOCK HOOK 13CAG	NFA	NF		1
15		NFB	NF		1
	DOWNLOCK HOOK 13CAJ				
02	COLLAR LOCKING AND SPRING 13CAL WHEEL STOP BUMPER 11ACA	NFC NFD	NF NF		0
02		NEE	NF		Ö
15		NFF	NF		C
02			NF		0
112	SOUAT SWITCH 13CCC	NEG			
115	EXTEND ACTUATION	NG	NA NUL		AAAAAAAA
115	EXTEND ACTUATION	NG NGA	NU NG		FAAAAAAAAA
15	LDG CONTROL 13AAA LINKAGE 13AAB	NGB	NG		8
72	LINKAGE 13AAB HANDLE UP-DOWN SWITCH 13ACB	NGC	NG		Δ .
-		NGD	NG		8
112	ACTUATOR DWNLOCK MN GEAR 13888 ACTUATOR UPLOCK RELEASE 13880	NGE	NG		g g
	HOSE MN STRUT DOOR OPEN 138PE	NGF	NG		1
02	HOSE LN MN GR DWNLOCK LOCK 13884	NGG	NG NG		
02	HOSE RH MN GR DWNLOCK LOCK 13680	NGH	NG NG		
12	ACTUATOR UPLOCK REL NOSE 13CHC	NGJ	NG		9
112	HOSE NOSE STRUT ACT EXTENDISCHO	NGK	NG		1
12	NORMAL PRESSURE	NJ	NC	NK	111111111
112	HYDRAULIC PUMP 13AHC	ALM	NJ		Δ
1.2	EMERGENCY PRESSURE	NK	NC NC	K NJ	AAAAAAAA
12	HAND PUMP EMERGENCY 13ABE	NKA	NK		A A A A A A A A A A A A A A A A A A A
-15	LEVER-EMERGENCY HAND PUMP 13APF	NKR	NK NK		A
-		NL	ND		
15	RETRACT ACTUATE	NL	NU		AAAAAAAA
112	PETRACT ACTUATE	NLA	NL NL		FILITITI
.15	LDG CONTROL 13AAA LINKAGE 13AAB	NLB	NL NL		8
12		NLC	NL NL		A
32	HANDLE UP-DOWN SWITCH 13ACB HOSE LH MN GR DWNLCCK UNLK1368K	NLO	NL NL		
0.5	HOSE LH MN GR DWNLOCK UNLKIBER	NLE	NL NL		
n2	HUSE RH MN GR DWNLOCK UNLK1388N	NLF	NŁ		
112	HOSE RH MN GR DWNLOCK UNLK138BP	NLG	VL VL		
	HOSE WELL MIA OF MARKETON OMENTOUS	145.0			

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	00000011111111112222222222233 4567890123456789012345678901					
112	HUSE NOSE STRUT ACT RETRAC		NLH	NL		1
.12	NOSE GEAR AND DOORS UP		NM	ND		AAAAAAAA
112	UPLOCK HOOK	13CAG	NMA	NM		1
112	DOWNLOCK HOOK	13CAJ	NMB	NM		1
112	COLLAR LUCKING AND SPRING		NMC	N:M		A
112	WHEEL STOP HUMPER	11ACA	NMD	NM		0
112	DOOR ASSY	13DAF	NME	NM		0
92	CIRCUIT BREAKER	42FAB	NMF	NM		A
02	SQUAT SWITCH	13000	NMG	NM		0
112	MAIN GEAR AND DUORS UP	•	NN	ND		AAAAAAAA
012	SADDLE	13844	NNA	NN		0
(12	DOWNLOCK HOOK	13BAD	NNS	NN		1
U2 .	DOWNLOCK ADJ SUPPORT	13BAF	NNC	NN		8
112	UPLOCK HOOK	138AJ	NND	NN		1
.12	U JOINT ASSY ZEA	136AL	NNE	NN		Ā
6.2	LINKAGE 2FA	13PAM	NNE	NN		ì
1.2	DOOR ASSY ZEA	13044	NNG	NN		0
02	DOOR ASSY STRUT 2EA	130AB	NNH	NN		0
112	HOSE MAIN STRUT DR CLOSED	-	NNJ	NN		1
112	LDG UNSAFE INDICATION		NU	NA	I NG	111111111
112	SWITCH WNG HORN DISABLE	13ACE	NUA	NU		1
02	SWITCH GEAR WNG THROTTLE	13ACF	NUR	NU		i
02	GEAR TRANSIT AND UP LIGHT	The state of the s	NUC	NU		ì
02	GEAR DOWN LIGHT	13ACH	CUN	NU		i
32	RELAY GO DISABLE WNG HORN		NUE	NU		î
* 62	SWITCH-UPLOCK MAIN GEAR	13BCA	NUG	NU		ì
02	SWITCH-DOWNLOCK MAIN GEAR	and the state of t	NUH	NU		
.)2	SWITCH UPLOCK	13CCA	NUJ	NU		ì
1:2	SWITCH-DOWNLOCK NOSE GEAR	Action Control of the	NUK	NU		i
02	CIRCUIT BREAKER ZEA	42FAB	NUL	NU		ì
12	WARNING RELAY &GD DISABLES		NUM	NU		ò
12	SOVA AC DIST	•	UAA	CCO		ΑΑΛΑΛΑΑΑ
72	SOVA AC DIST		UAA	CCF		FAAAAAAAAA
112	SOVA AC DIST		UAA	CCH		FAAAAAAAAA
12	SUVA AC DIST		UAA	CCJ		FAAAAAAAAA
22	60VA AC DIST		UAA	CCP		AAAAAAAA
	GOVA AC DIST		UAA	cco		SAAAAAAAAA
	60VA AC DIST		UAA	CCR		FAAAAAAAAA
	60 VA AC DIST		UAA	CCT		FAAAAAAAAA
1)213			UAA	CCT		AAAAAAAA
024	GOVA AC DIST		UAA	00		ΑΑΑΑΑΑΑΑ
ASU	SELECTOR SWITCH INVERTER	9942A	UAAA	UAA		5
1128	INVERTER	42FAG	UAAB	UAA		A
128	CKT BKR GYRO POWER	42FAR	UAAC	UAA		A
110.00	60 VA AC SVS NO 1		UAB		K UAC	AAAAAAAA
ASO	INVERTER	42FAG	UARA	UAB		A
ASC	CKT BKR INV PWR NO 1	42FAB	UARB	UAB		A
	60 VA AC SVS NO2		UAC		K UAR	AAAAAAAA
ASI	INVERTER	42FAG	UACA	UAC		4
112A	CKT BKR INV PWR NO 2	42FAB	UACB	UAC		A

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	1111	DAIL	-	01,12	, , ,

123	00000011111111111222	22222223	3333333	3344444444	445555555555666666	666677777777778
22	400 VA AC DIST			UAD	CRA	AAAAAAAA
12	400 VA AC DIST			UAD	CCD	AAAAAAAA
02	CKT BKR		42FCD	UADA	GAU	A
112	INVERTER	42FAJ	42FAH	UADB	UAD	A
02	INVERTER	42FAH	42FAJ	UADC	UAD	A
024	RELAY INVERTER		42FCH	UADO	UAD	8
65	PRIMARY DC BUS			UDA	LBHX	FAAAAAAAA
02	PHIMARY DC BUS			UDA	RBHX	FAAAAAAAA
32	PRIMARY DC BUS			UDA	LBJX	AAAAAAAA
02	PRIMARY DC HUS			UDA	XLBP	AAAAAAAA
02	PRIMARY DC BUS			AOU	LBKA	AAAAAAAA
:12	PRIMARY DC BUS			UDA	RBKA	AAAAAAAA
02	PRIMARY DC BUS			UDA	LBN	AAAAAAAA
nz	PRIMARY DC BUS			ACU	RBN	AAAAAAAA
02	PRIMARY DC BUS			UDA	LBRF	AAAAAAAA
02	PRIMARY DC BUS			UDA	RBRF	AAAAAAAA
72	PRIMARY DC BUS			UDA	LBSC	AAAAAAAA
02	PRIMARY DC BUS			NCU	PASC	AAAAAAAA
02	PRIMARY DC HUS			UDA	CAL	AAAAAAAA
02	PRIMARY DC BUS			UDA	DL	AAAAAAAA
02	PRIMARY DC BUS			UDA	DP	AAAAAAAA
02	PRIMARY DC BUS			UDA	DU	AAAAAAAA
72	PRIMARY DC BUS			UNA	DV	FAAAAAAAAA
112	PRIMARY DC BUS			UDA	EA	AAAAAAAA
02	PRIMARY DC BUS			UDA	FAF	AAAAAAAA
1321	PRIMARY DC BUS			UDA	FCG	AAAAAAA
124	PRIMARY DC BUS			UDA	MAG	AAAAAAAA
CIZA	PRIMARY DC BUS			UDA	LAM	AAAAAAAA
12A	PRIMARY DC BUS			UDA	MB	AAAAAAAA
1124				UDA	MC	ΑΔΑΔΑΔΑΔ
112	PRIMARY DC BUS			UDA	NF	000000000
112	PRIMARY DC BUS			UDA	NL	AAAAAAA
112	PRIMARY DC POWER			AGU	NU	ΑΛΑΑΑΑΛΑ
1124	PPIMARY DC HIS			ACU	UAA	SAAAAAAAA
028				UDA	UAA	AAAAAAAA
DZA	PRIMARY DC BUS			UDA	HAU	FAAAAAAAA
1124				UDA	UAC	FAAAAAAAA
02	PRIMARY DC BUS			UDA	UDH	+ 44444444
0.2	JUNGTION BOX FWD		42FB0	UDAA	UDA	1
62	TERMINAL STRIP		42F88	UDAB	UDA	ò
112	CKT BKR PANEL		42FAF	UDAC	UDA	Ö
12	RELAY		42FAD	UDAD	UDA	Ö
112	JUNCTION BOX REAR		42FC0	UDAE	UDA	i
112	TERMINAL STRIP		42FCE	UDAF	UDA	0
112	FILTER		42FCB	UDAG	UDA	0
028	VOLTMETER		42GAA	UDAH	UDA	Č
02	DC ELECTRONICS DIS		72004	UDB	CAH	SAAAAAAAA
02	DE ELECTRONICS DIS			UDA	CAD	
12	DC ELECTRONICS DIS			UDB	CAE	FAAAAAAAAA
112	DC ELECTRONICS DIS			UDA	CAF	FAAAAAAAA
	OC EFFCINOAICS DIS			Oth	CHI	Гимиминия Пимиминия

FLIGHT SAFETY PREDICTION TECHNIQUE PGG095. J1 R1 DATE = 01/12/76 12345678901234567890123456789012345678901234567890123456789012345678901234567890 CAG DC ELECTRONICS DIST UDB FAAAAAAAA 02 UDB CB SAAAAAAAA 02 DC ELECTRONICS DIST 02 DC ELECTRONICS DIST UDB CBA FAAAAAAAA CZA OC ELECTRONICS DIST UDB CBB FAAAAAAAAA 577777777 112 **ELECTRONICS DIST** UDB CCB ELECTRONICS DIST UDB CCD FAAAAAAAAA 12 DC 12 ELECTRONICS DIST UDB CCM FAAAAAAAAA MD AAAAAAAA UDB 128 DC ELECTRONICS DIST ELECTRONICS UDB UAD AAAAAAAAA DC 112 JUNCTION BOX REAR 42FCO UDBA UDS TERMINAL STRIP 42FCE UDBB 02 UDB 0 92 FILTER 42FCB UDBC UDB C2B ELECT DISABLE CONTACTOR 99420 UDBD UDB (12 NORMAL SOURCE UDC UDA UDE 111111111 UDC UDK NORMAL SOURCE ...... 112 LUDD KRUDD AAAAAAAA 02 FRONT ALT SUPPLY UDC KLUDD 02 REAR ALT SUPPLY RUDD UDC AAAAAAAA 112 GEAR DRIVEN ALT 42AAA LUDDA LUDD 02 GEAR DRIVEN ALT 42AAA RUDDA RUDD A DRIVE 02 42 AAB LUDDR LUDD Δ 42 AAB RUDDB RUDD 72 DRIVE ALT ASSY BELT DRIVEN 42AAE RUDDC RUDD 02A ARM ALT ADJUST 42AAF RUDDD RUDD 1 024 HELT ALT DRIVE 42AAG RUDDE RUDO 1124 SUPPORT RUDDF RUDD ASSY 42 AAH 021 1 SHOCK MOUNT 42AAJ RUDDG RUDD 024 PULLEY PROP SHAFT 42AAK RUDDH RUDD 124 ALTERNATOR SWITCH LUDD 12 42CAA LUDDJ A 112 ALTERNATOR SWITCH 42CAA RUDDJ RUDD 12 CKT BKR 42FAB LUDDK LUDD A :12 CKT BKR 42FAB RUDDK RUDD ALT SHUNT LUDDL LUDD 12 42FAC 172 42FAC RUDDL RUDD ALT SHUNT 42CAF LUDO 02 SUPPRESSOR LUDDM 12 SUPPRESSOR 42CAF RUDDM RUDD K UDC 02 EMERGENCY SOURCE UDE UD4 AAAAAAAA BATTERY SHUNT 42FAC UDEA UDE 12 32 BATTERY SHUNT 42FAC UDEA UDK CONTROL/REGULATION 1.23 UDF UDC ...... CONTROL/REGULATION LUDF LUDD AAAAAAAAA 12A ..... ASC CONTROL/REGULATION RUDE RUDD UDF UDFA 228 VOLTAGE REGULATOR \$2EAC 42CAC DZA VOLTAGE REGULATOR 42CAC LUDFA LUDF 8 VOLTAGE REGULATOR 42 CAC RUDFA RUDF 724 8

UDFB

LUDFB

RUDFB

UDG

UDG

UDFC

UDF

LUDF

RUDF

HIDE

UDC

LUDD

0

0

SAAAAAAAAA

FAAAAAAAAA

42GAB

42GAB

42 GAB

42CAD

28

024

123

172A

AMMETER

AMMETER

AMMETER

SWITCH REG SELECT

FIELD CURRENT SOURCE

FIELD CURRENT SOURCE

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FLIGHT SAFETY PREDICTION TECHNIQUE

	45678901234567890123456789	101234301		RUDD	2343011	FAAAAAAAA
ASD	FIELD CURRENT SOURCE		UDG			
USB	FIELD CURRENT SOURCE		UDG	UDF		AAAAAAAA
02	OVERVOLTAGE RELAY	42GAG	UDGA	UDG		8
028	ALT RUN/STRY SW	42CAE	UDGB	UDG		
02	NORMAL SOURCE		UDH	UDG	UD.	, , , , , , , , , , , , , , , , , , , ,
02	ALT FIELD CKT BKR	42FAB	UDHA	UDH		A
02	BATT/MASTER SW	42EAE	UDHB	UDH		
02	EMERGENCY SOURCE		UDJ	UDG	K UD	
02A	RESTART SWITCH	42CAB	UDJA	UDJ		
024	RECT DIODES	42EAF	UDJB	กอา		,
028	DIODE	42EAF	UDJC	non		A
028	FUSE	99428	ODJO	UDJ		A
02	BUS-TO-BUS CONNECTION		UDK	UDB	UDI	
0.2	BATTERY CONNECTION		UDL	UDB	K UDI	
02	BATTERY CONNECTION		UDL	UDE		AAAAAAAA
72	BATTERY CONTACTOR	42 FAD	UDLA	UDL		A
02	DIODE	42EAF	UDLB	UDL		5
02	BATT/MASTER SWITCH	42EAF	UDLC	UDL		A
OZA	BATTERY SUPPLY		UDM	HAM		AAAAAAAA
OZB	BATTERY SUPPLY		UDM	UDJ		FAAAAAAAA
72	BATTERY SUPPLY		UDM	UDL		AAAAAAAA
02	BATT, LEAD ACID	42EAA	UDMA	UDM		6
024	BATT NICAD	42EAH	UDMB	UDM		6
02	BATT BOX	42FAC	UDMC	UDM		0
72	EXTERNAL POWER		UDN	UDB		000000000
02	EXTERNAL POWER		UDN	UDE		000000000
02	RECEPTACLE	42FAA	UDNA	UDN		8
DZA	CONTACTOR	42FAK	UDNB	UDN		A
OZA	DIODE	9942F	UDNC	UDN		A
DZA	RESISTOR, EXT POWER	9942E	UDND	UDN		A
DZA	FUSE EXT POWER	99420	UDNE	UDN		

CARD COUNT IS 00001380. CARDS WITH ERRORS 00000000